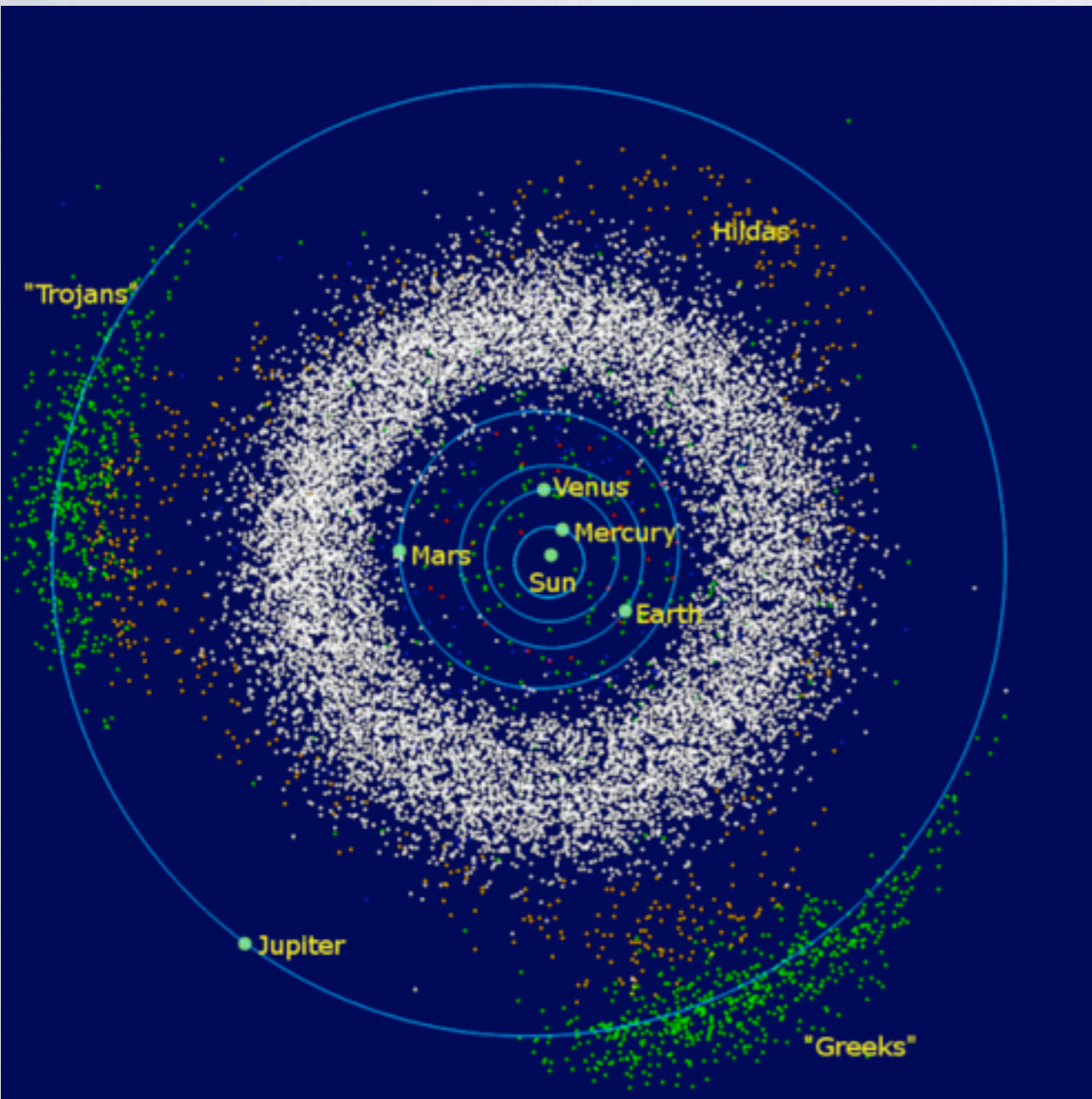


*Cracking and crushing:
Modeling the collisional history
of small bodies in the solar
system*

W. Benz
University of Bern
Switzerland

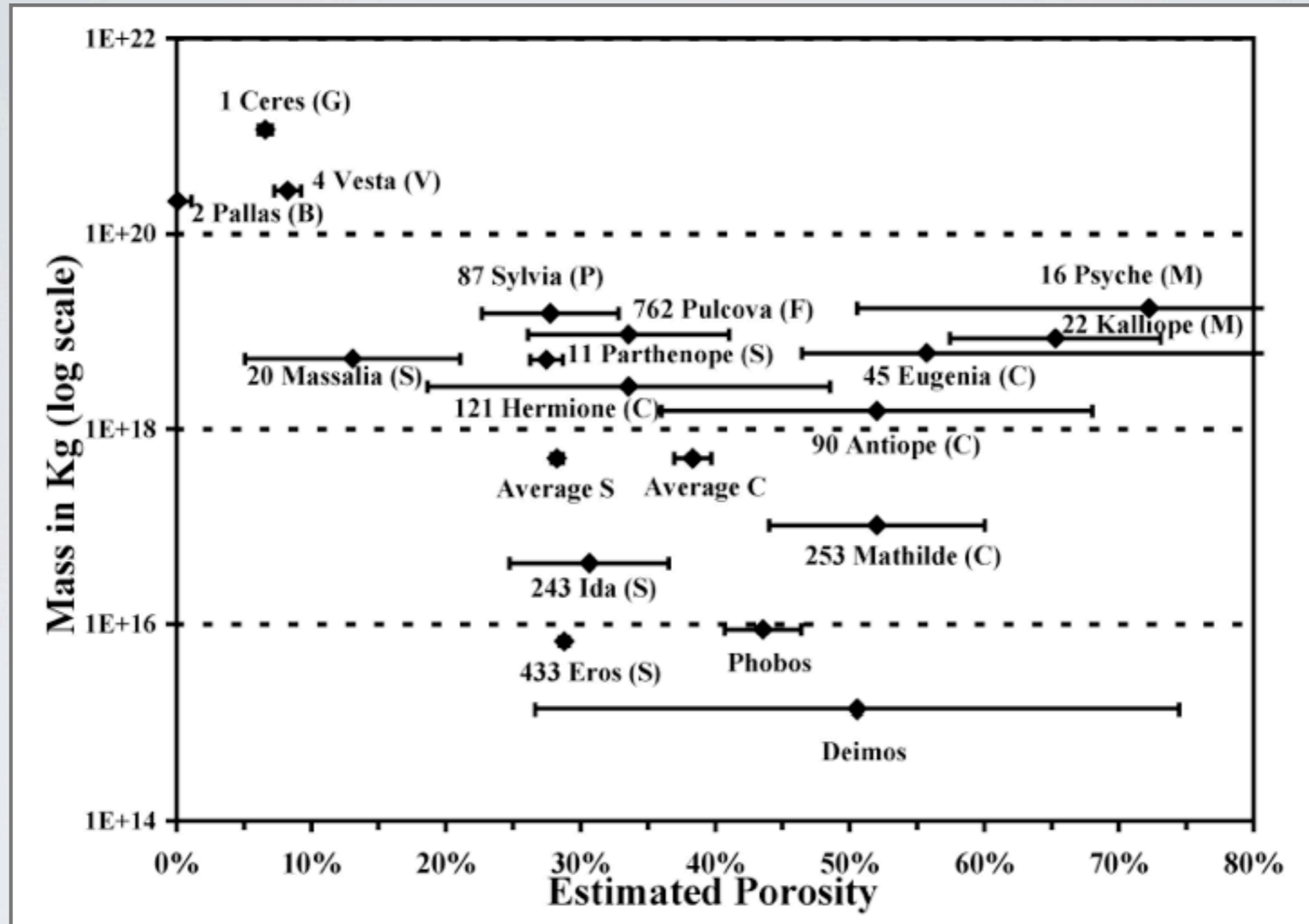
Small bodies: The asteroid population



Fact sheet:

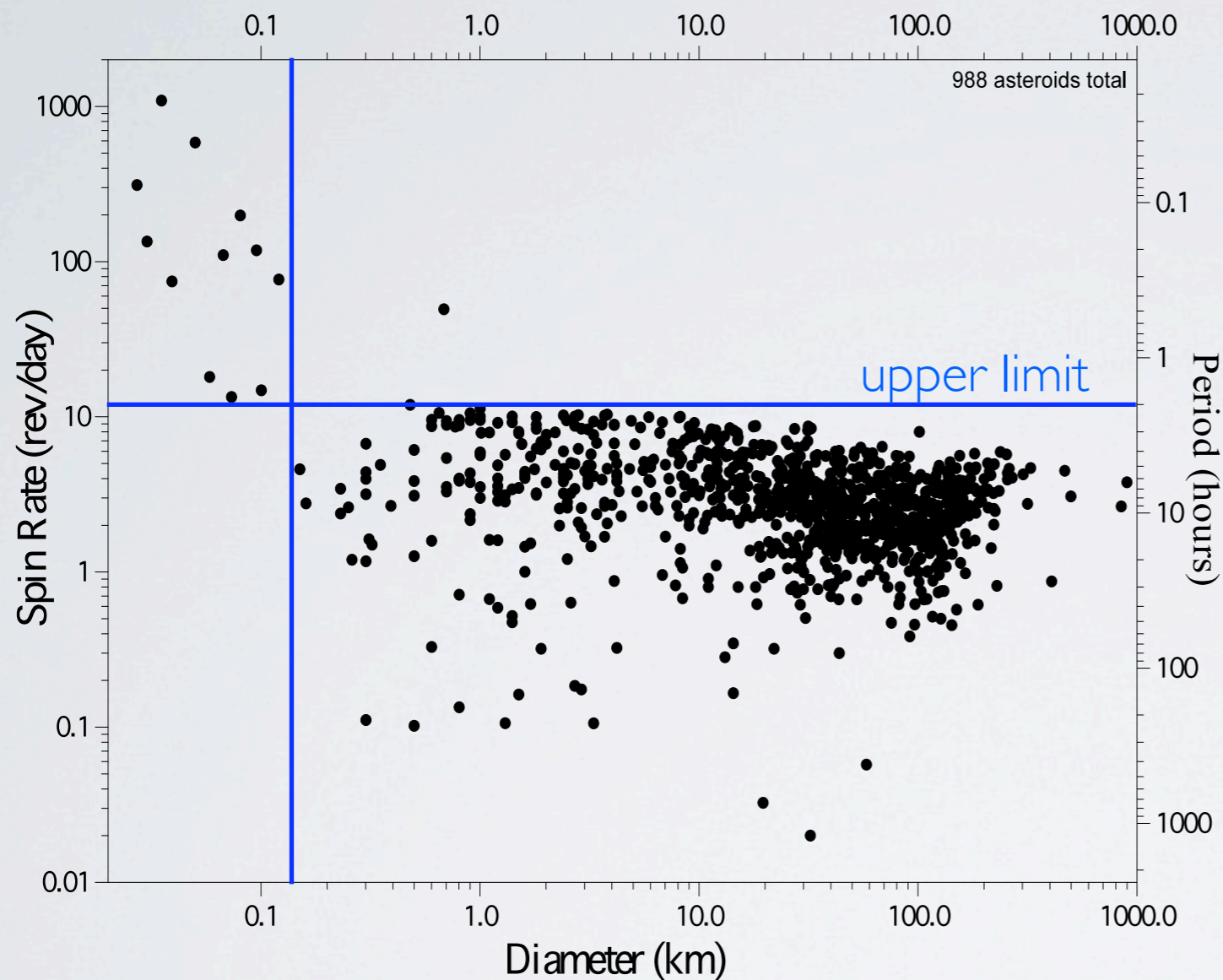
- estimated number: $1.1-1.9 \cdot 10^6$ with diameter > 1 km
- estimated total mass: 4% of a lunar mass
- orbits located mainly between Mars and Jupiter
- largest object: Ceres $D=950$ km

Mean density of asteroids

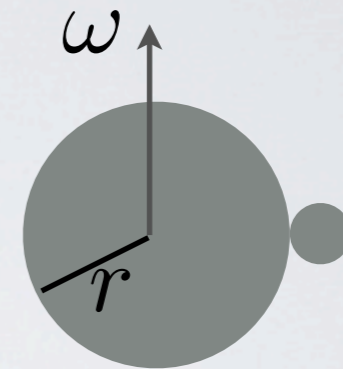


there is considerable evidence that asteroids are porous bodies...

Rotation rate of asteroids



rubble pile speed limit:



gravity = centrifugal force

$$\omega = \sqrt{\frac{Gm}{r^3}} = \omega_0 \sqrt{\rho}$$

→ limit independent of size...

there is considerable evidence that large asteroids are rubble piles...

*Meet the small
and famous...*

Meet the small and famous...



253 Mathilde
66 x 48 x 44 km
Near 1997



243 Ida
59 x 25 x 19 km
Galileo 1993



433 Eros
33 x 13 km
Near 2000



951 Gaspra
18 x 11 x 9 km
Galileo 1993

Dactyl
1.6 x 1.2 km
Galileo 1993



1P/ Halley
16 x 8 x 8 km
Vega 2 1986



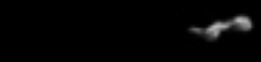
19P/ Borelly
8 x 4 km
Deep Space 1 2001



5535 Annefrank
7 x 5 x 3 km
Stardust 2002



2867 Steins
6 x 5 x 5 km
Rosetta 2008



9969 Braille
2 x 1 x 1 km
Deep Space 1 1999



9P/ Tempel 1
8 x 5 km
Deep impact 2005



81P/ Wild 2
6 x 4 x 3 km
Stardust 2004

253 Mathilde

66 x 48 x 44 km

Near 1997



mean density: 1.3 g cm^{-3}



2867 Steins

6 × 5 × 5 km

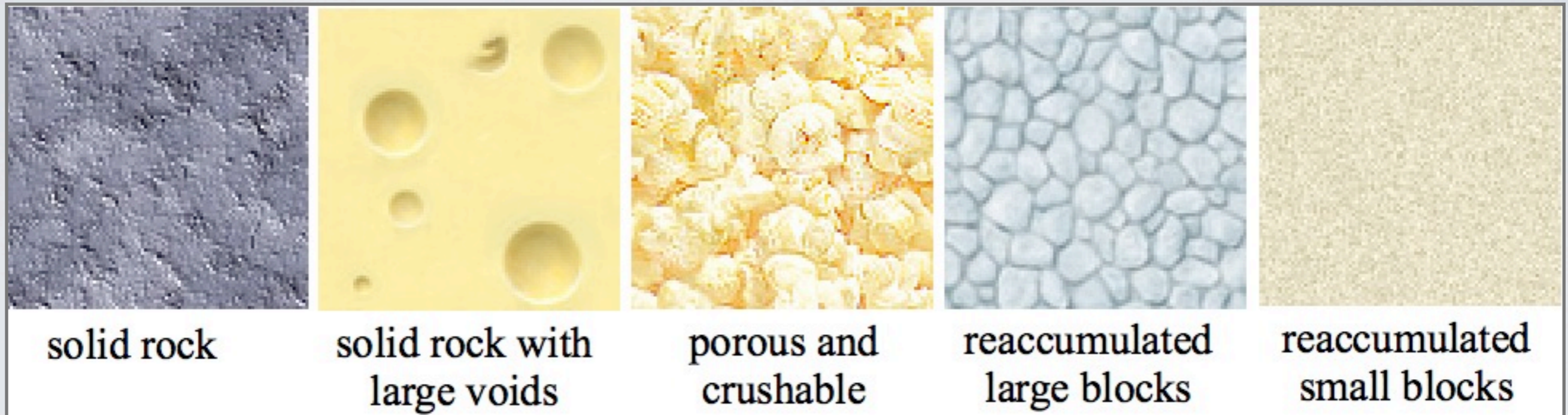
Rosetta 2008

A diamond in the sky....

Modeling solid materials

(for planetary science applications)

What is out there:



the material characteristics will determine the response to impacts and hence will determine the evolution of the bodies

Fracture

- explicit flaw distribution: Weibull distribution

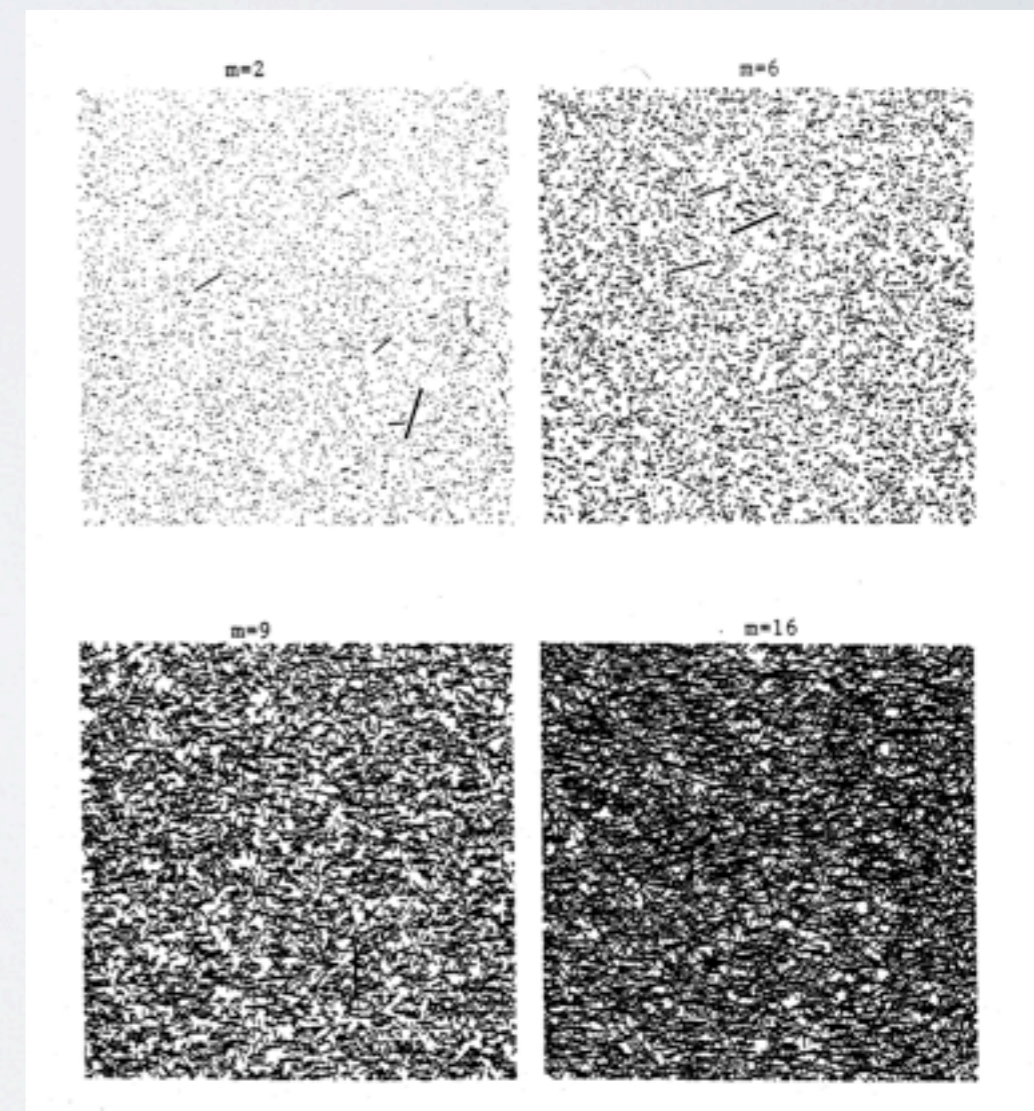
$$n(\epsilon) = k\epsilon^m \quad \text{with } n(\epsilon) \text{ the number density of active flaws at strain } \epsilon$$

k, m material parameters

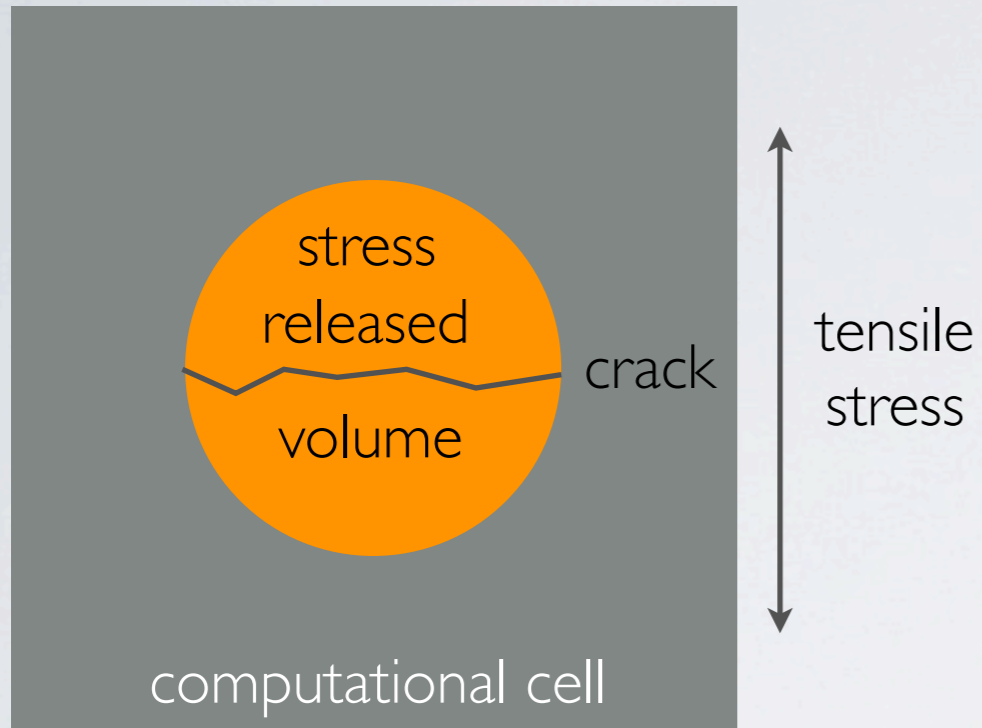
- flaw activation threshold

$$\epsilon_i = \left(\frac{i}{kV} \right)^{1/m} \quad i = 1, 2, \dots, N$$

activation thresholds are distributed randomly over all particles



Damage: feed-back on the dynamics



Damage growth:

$$D(t) = \frac{V(t)}{V_{cell}} = \frac{\frac{4}{3}\pi c_g(t - t_0)}{V_{cell}}$$

with: t_0 the activation time
 c_g the crack growth speed

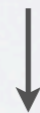
$$0 \leq D \leq 1$$

intact



full tension and shear

entirely damaged



no tension or shear

*Damage is the result of the entire stress history of a solid
→ the Lagrangian nature of SPH is essential*

Comparison with experiments

→ sailor hat experiment (1965):

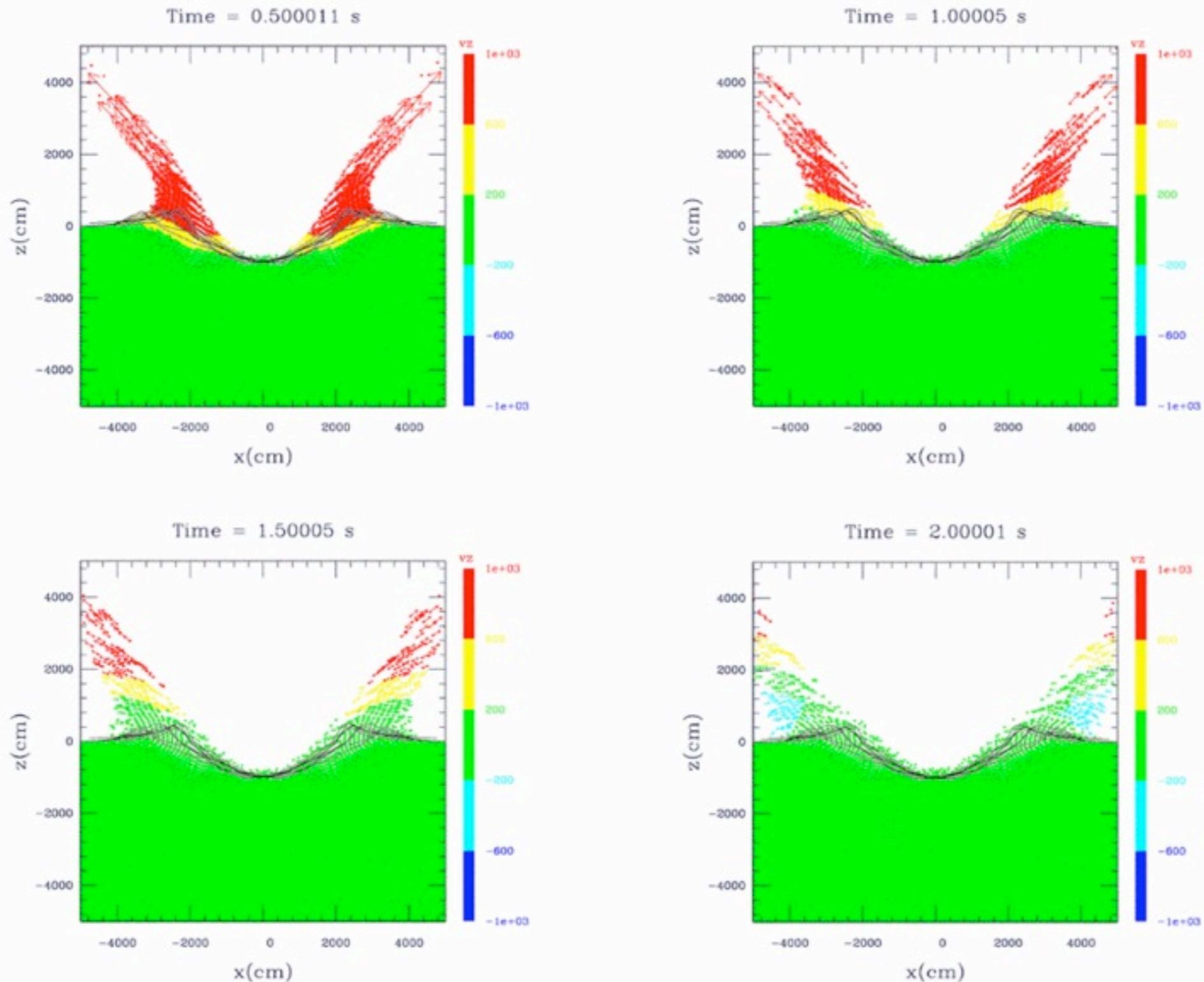
$4.54 \cdot 10^8$ g of TNT detonated on Kahoolawe Island (Hawaii): $4.2 \cdot 10^{10}$ ergs



crater diameter: 88.4 m

Sailor hat simulations

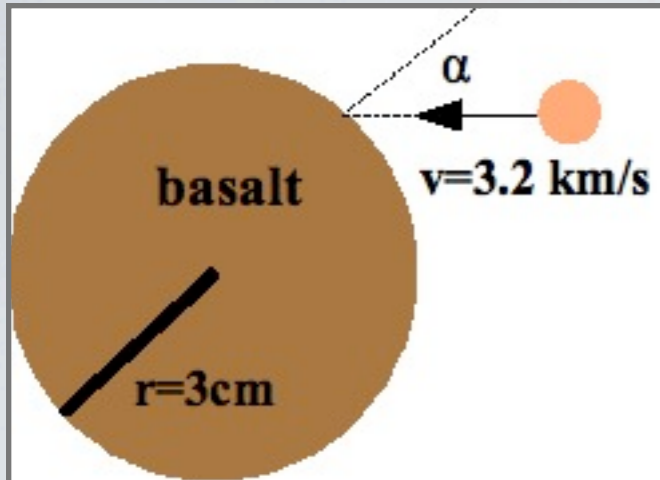
SPH simulations using 2.5×10^6 particles



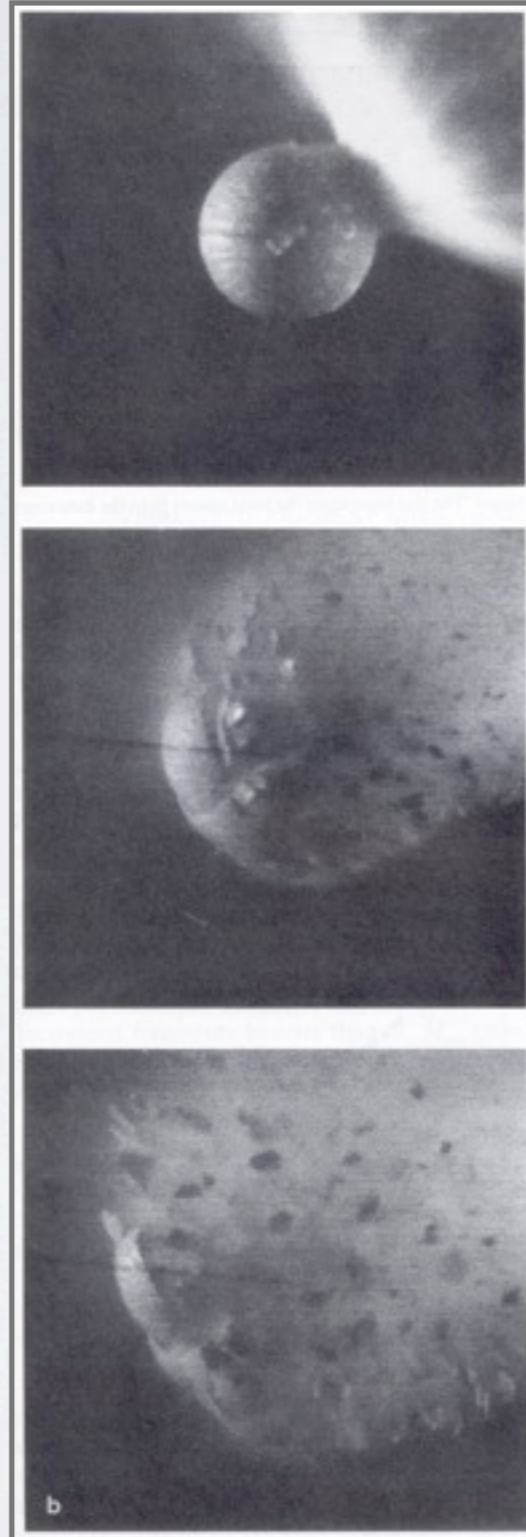
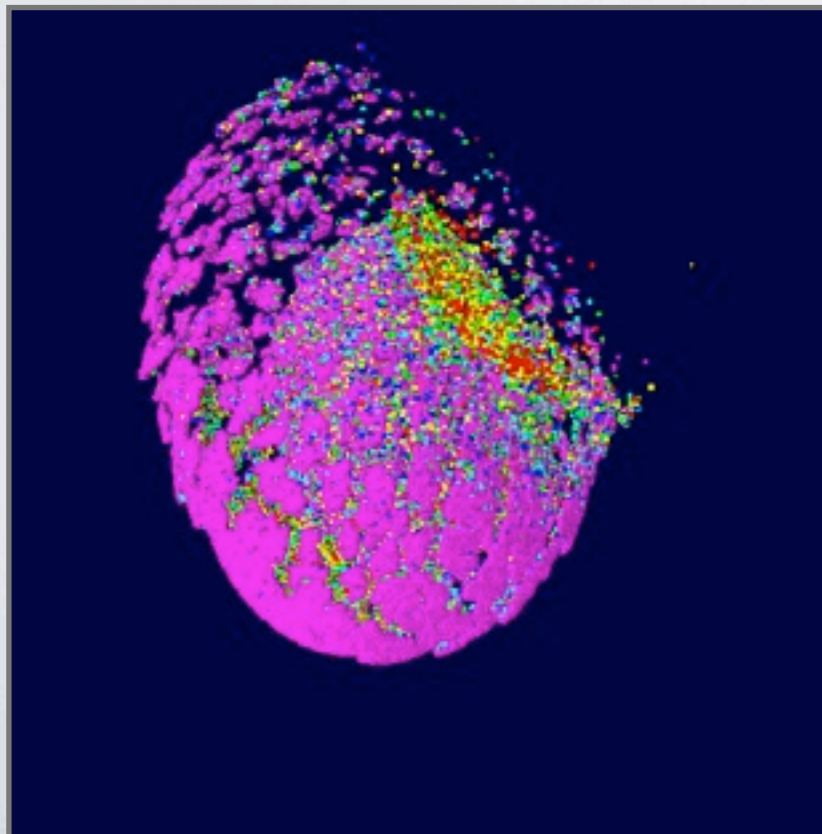
Comparison with impact experiments

→ SPH simulations using 3×10^6 particles

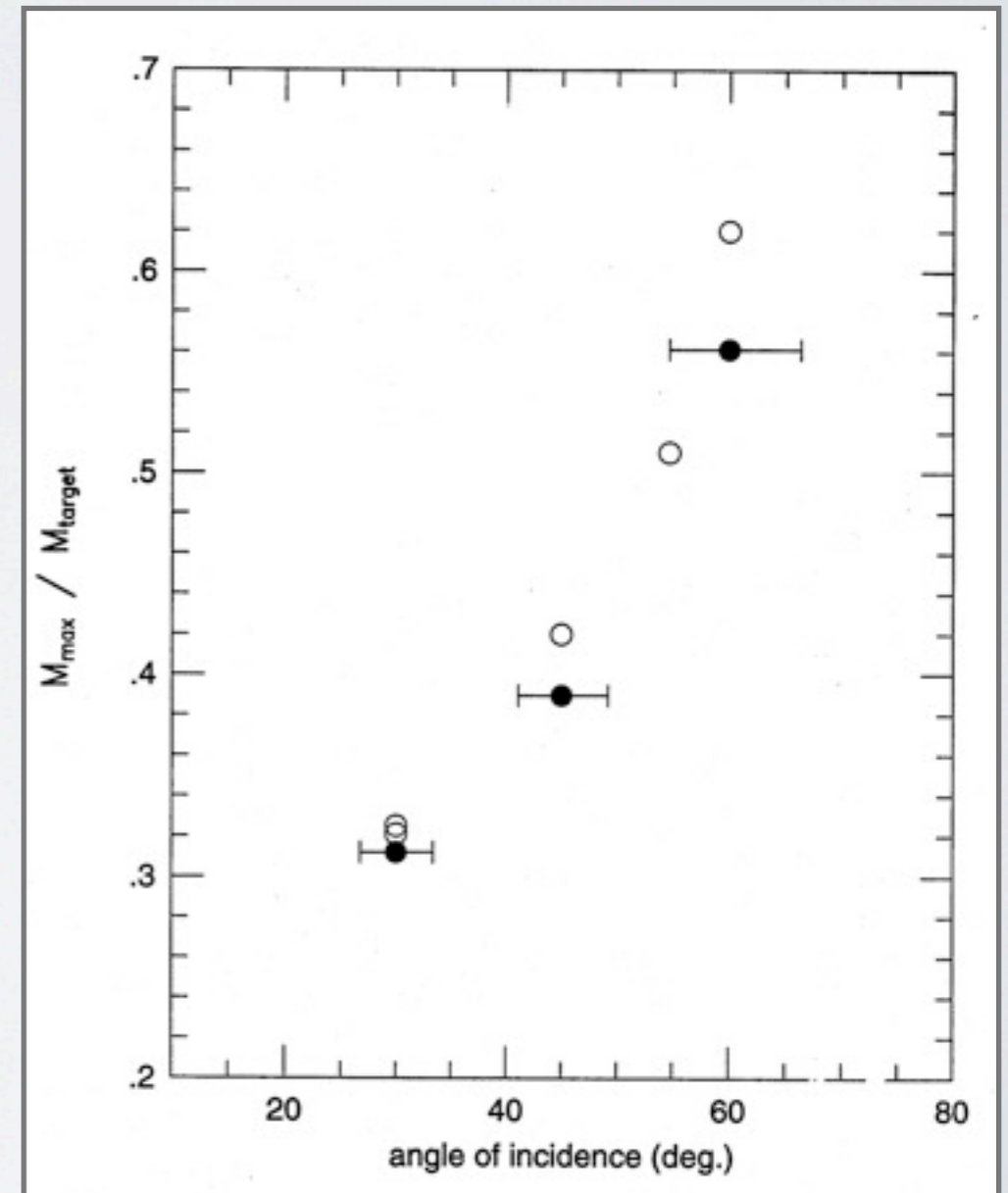
Nakamura & Fujiwara 93



dust removed



largest fragment as a function of impact angle



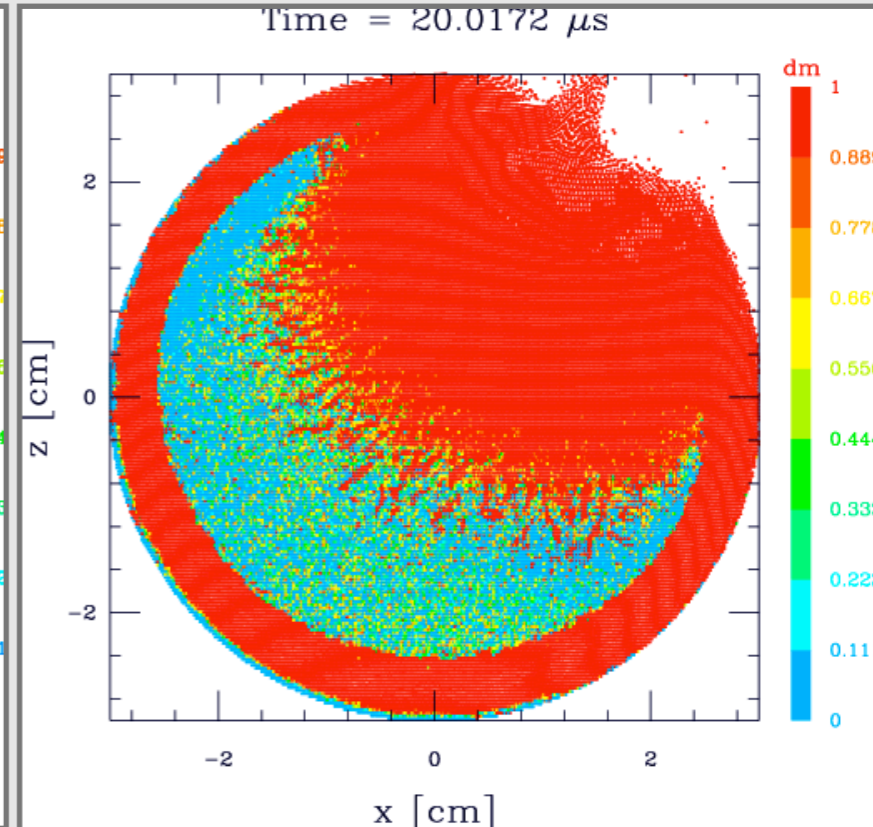
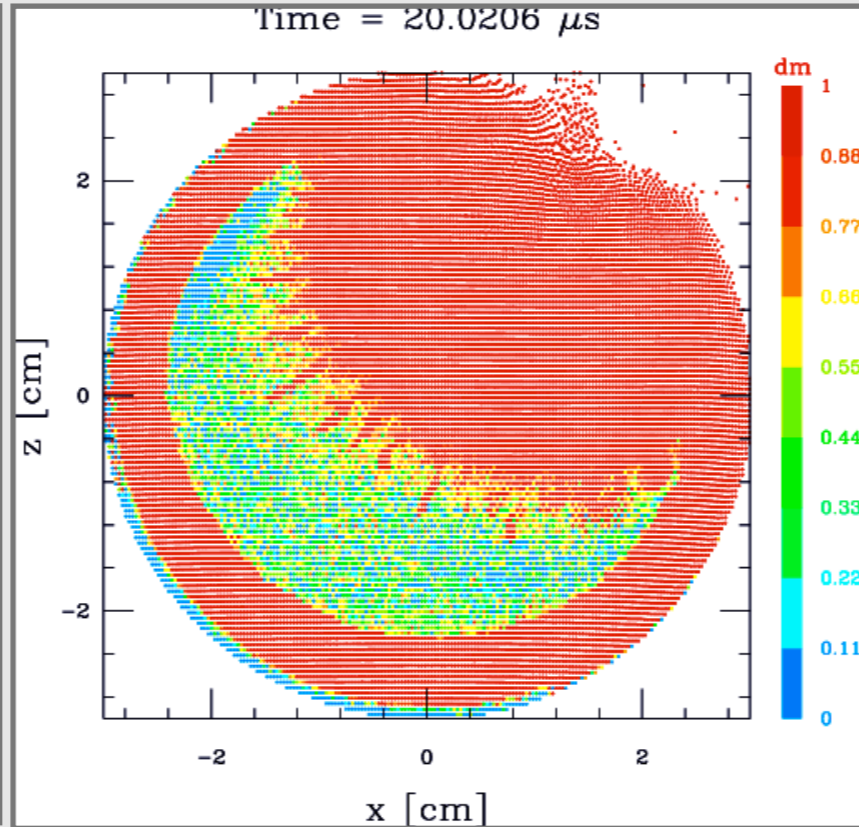
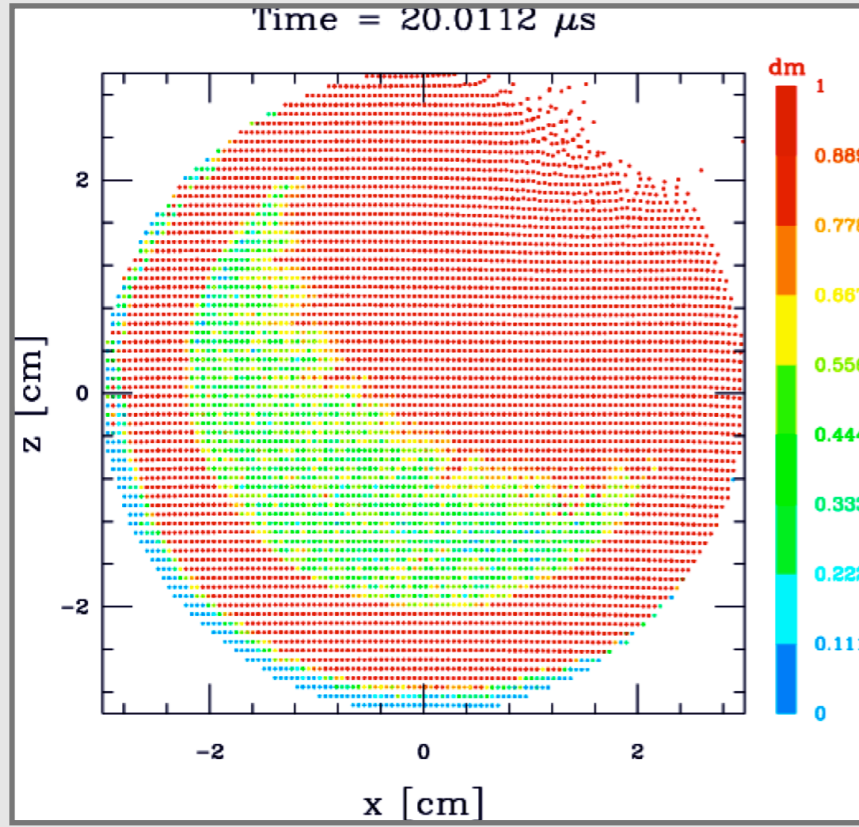
Convergence

$N=140'000$
 $h=0.104$ cm

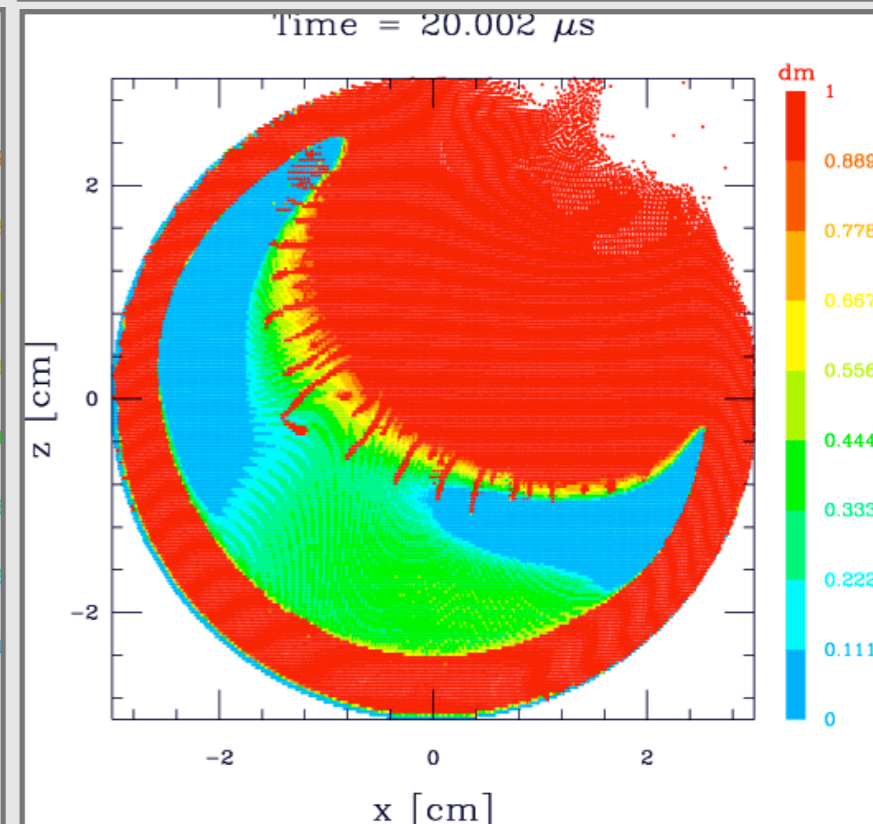
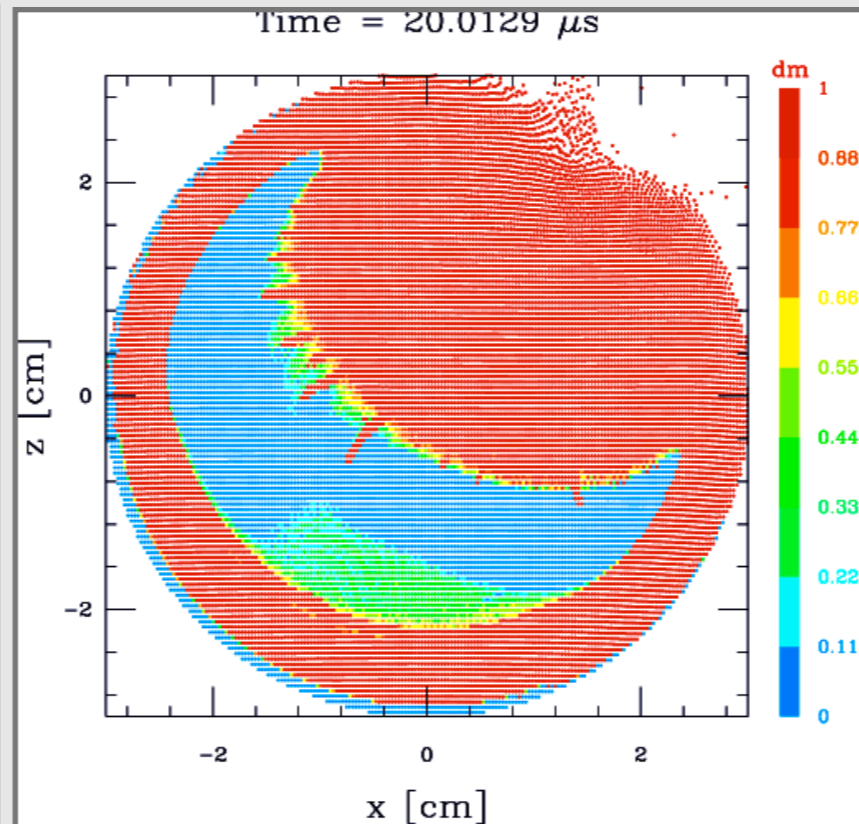
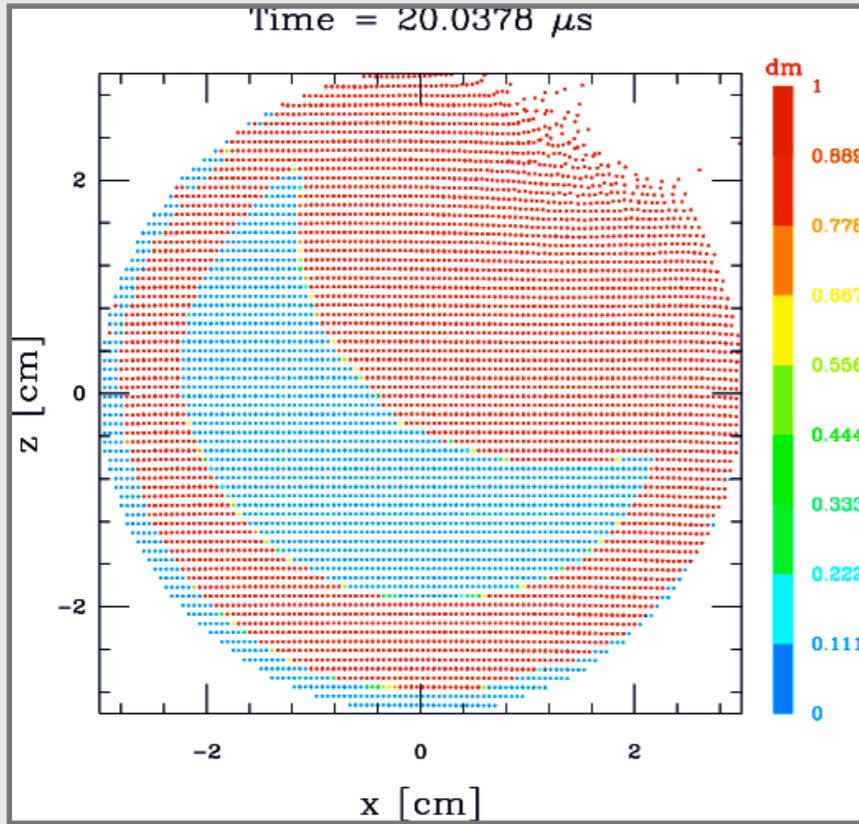
$N=700'000$
 $h=0.061$ cm

$N=3'500'000$
 $h=0.036$ cm

$m=9.5$



$m=\infty$



Porosity

Definitions:

- porosity:

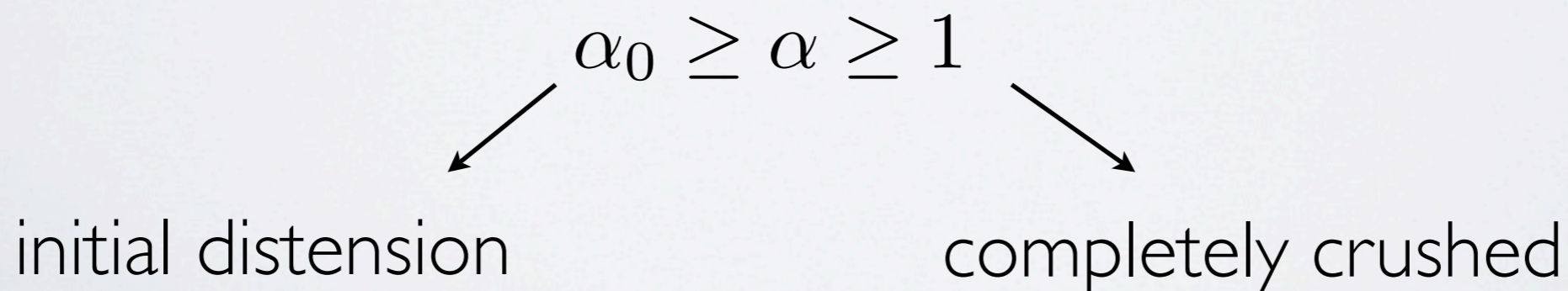
$$\phi = \frac{V - V_S}{V} = \frac{V_V}{V}$$

with V_S the volume of the matrix
 V_V the volume of the voids
 V the total volume

- distension:

$$\alpha = \frac{\rho_s}{\rho} = \frac{1}{1 - \phi}$$

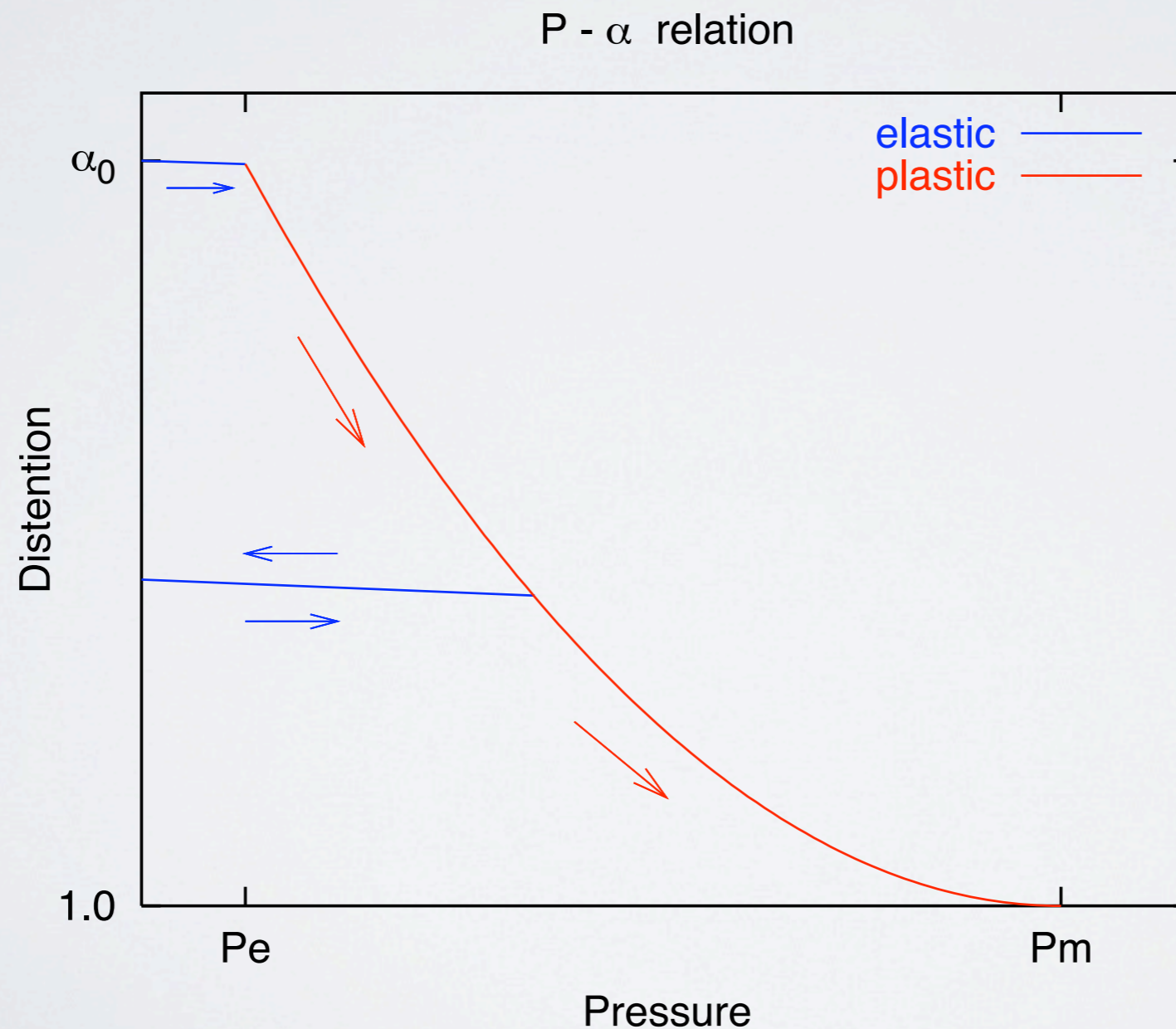
with ρ_s the density of the matrix
 ρ the bulk density



Crush curve

Distension is defined as a function of pressure: $\alpha = \alpha(P)$

the so-called $P - \alpha$ model (Hermann 1969)



Implementation

- Distension modifies the equation of state (eos):

$$P = \frac{1}{\alpha} P_s(\rho_s, E_s) = \frac{1}{\alpha} P_s(\alpha\rho, E) \quad \alpha = \frac{\rho_s}{\rho}$$

where $P_s(\rho_s, E_s)$ is the EOS of the solid phase of the material.

Several eos for solid material exist, e.g., Tillotson EOS, ANEOS, etc.

- Time evolution of distension:

$$\dot{\alpha}(t) = \frac{\dot{E} \left(\frac{\partial P_s}{\partial E_s} \right) + \alpha \dot{\rho} \left(\frac{\partial P_s}{\partial \rho_s} \right)}{\alpha + \frac{d\alpha}{dP} \left[P - \rho \left(\frac{\partial P_s}{\partial \rho_s} \right) \right]} \cdot \frac{d\alpha}{dP}$$

Distension: feed-back on the dynamics

- Distention and deviatoric stress

- ▶ Idea: compute the deviatoric stress as a function of the matrix variables

$$[\vec{\nabla} \vec{v}]_s = f[\vec{\nabla} \vec{v}] \rightarrow \frac{dS^{ij}}{dt} \rightarrow f \frac{dS^{ij}}{dt} \quad \text{where } f = 1 + \frac{\dot{\alpha} \rho}{\alpha \dot{\rho}}$$

- Distention and damage

- ▶ Since both damage D and distention α are volume ratios, we can relate the two by (linear relation):

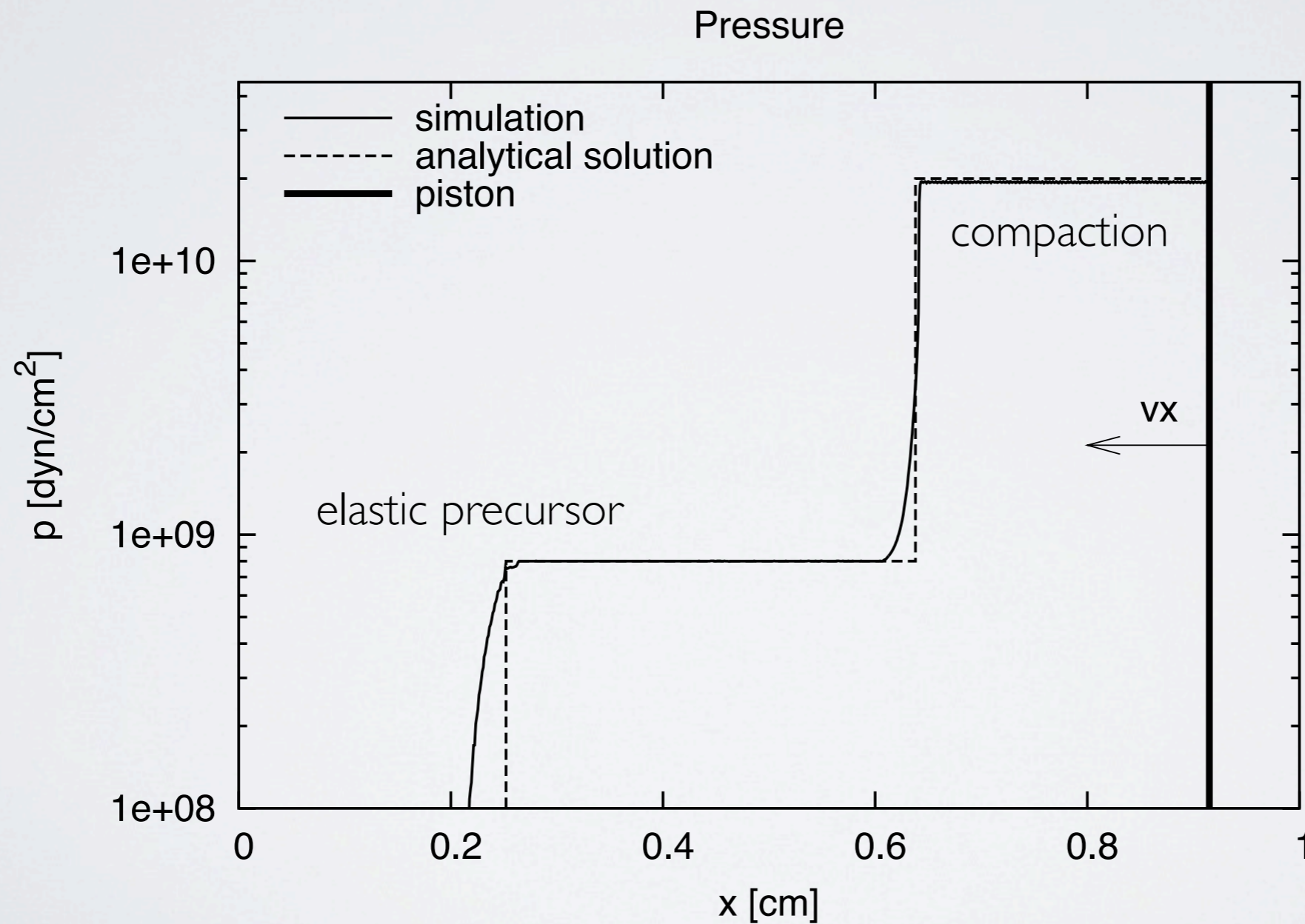
$$D = 1 - \frac{(\alpha - 1)}{(\alpha_0 - 1)}$$

$\alpha = 1 \rightarrow D = 1$

$$\begin{aligned} \text{total damage} = & \\ & \text{tension damage (Weibull flaws)} \\ & + \\ & \text{compression damage (breaking pores)} \end{aligned}$$

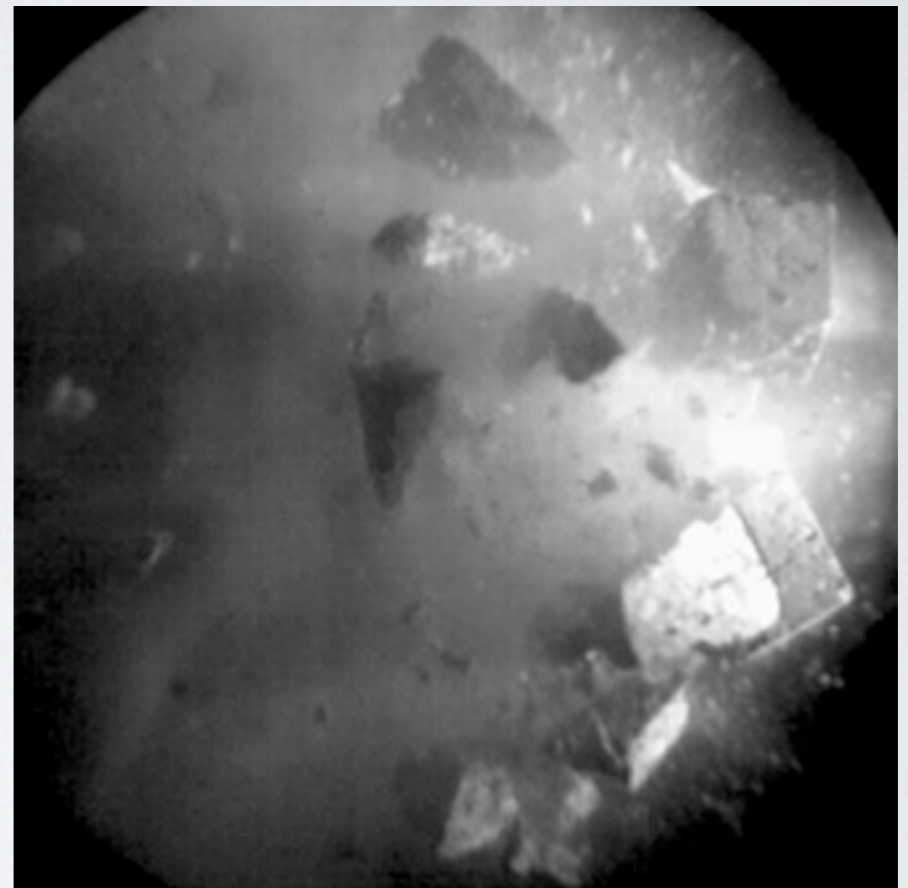
Simple test: Compaction wave

1D pressure wave



Comparison with laboratory experiments

- Experiments by A. Nakamura and K. Hiraoka (Kobe University) using a two stage light gas gun at ISAS
- Impact of nylon/glass projectile on porous pumice
- Measured material properties: Crush-curve, bulk density, tensile strength
- Measured quantities:
 - ▶ Mass distribution of fragments
 - ▶ Antipodal velocities
 - ▶ Snapshots of expanding fragments



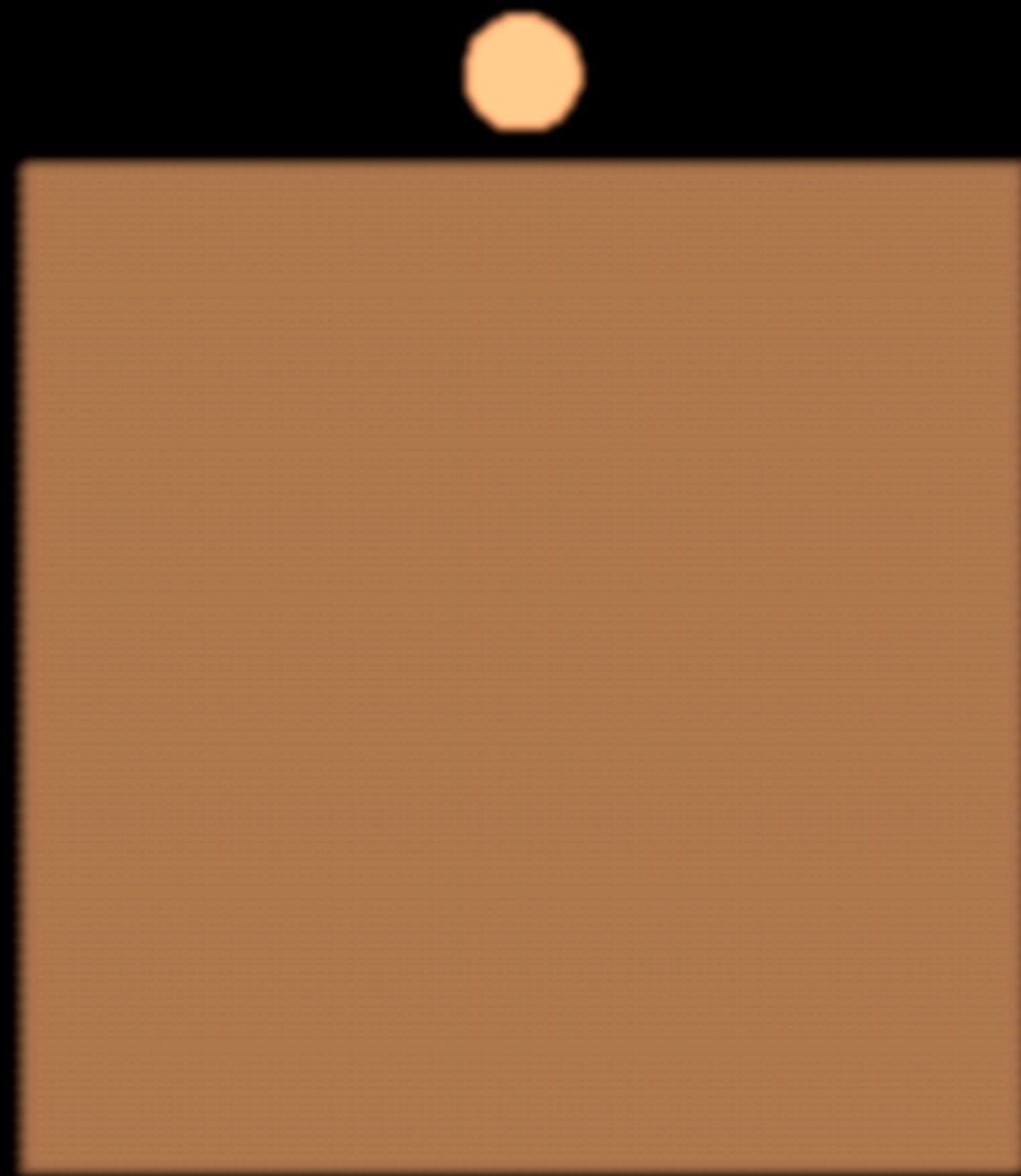
Comparison with laboratory experiments

Simulation of 4 shots:

Projectile					Target	
	Material	Diameter mm	Mass g	Velocity km/s	Mass g	Porosity %
418-4	Nylon	7	0.21	2.58	147.8	71
824-6	Glass	3.2	0.04	4.47	40.1	73
825-4	Nylon	7	0.21	3.28	38.7	75
70427	Nylon	3.2	0.02	3.94	37.3	75

Same material parameters (the measured ones) for all simulations

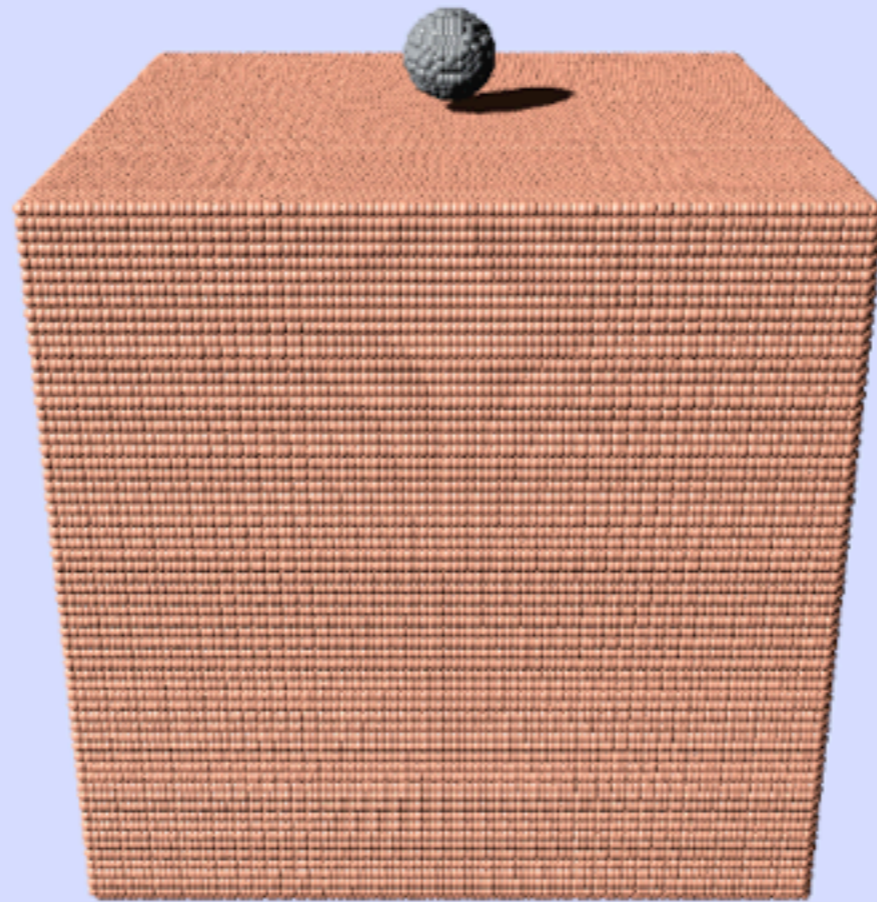
Number of particles:
 $1.4 \cdot 10^6$



6 cm

Evolution of damage
0 - 0.1 ms

Impact and subsequent expansion of fragments



Impact: 0 - 200 ms
Expansion: 0.2 ms - 16 ms

Comparison with laboratory experiments

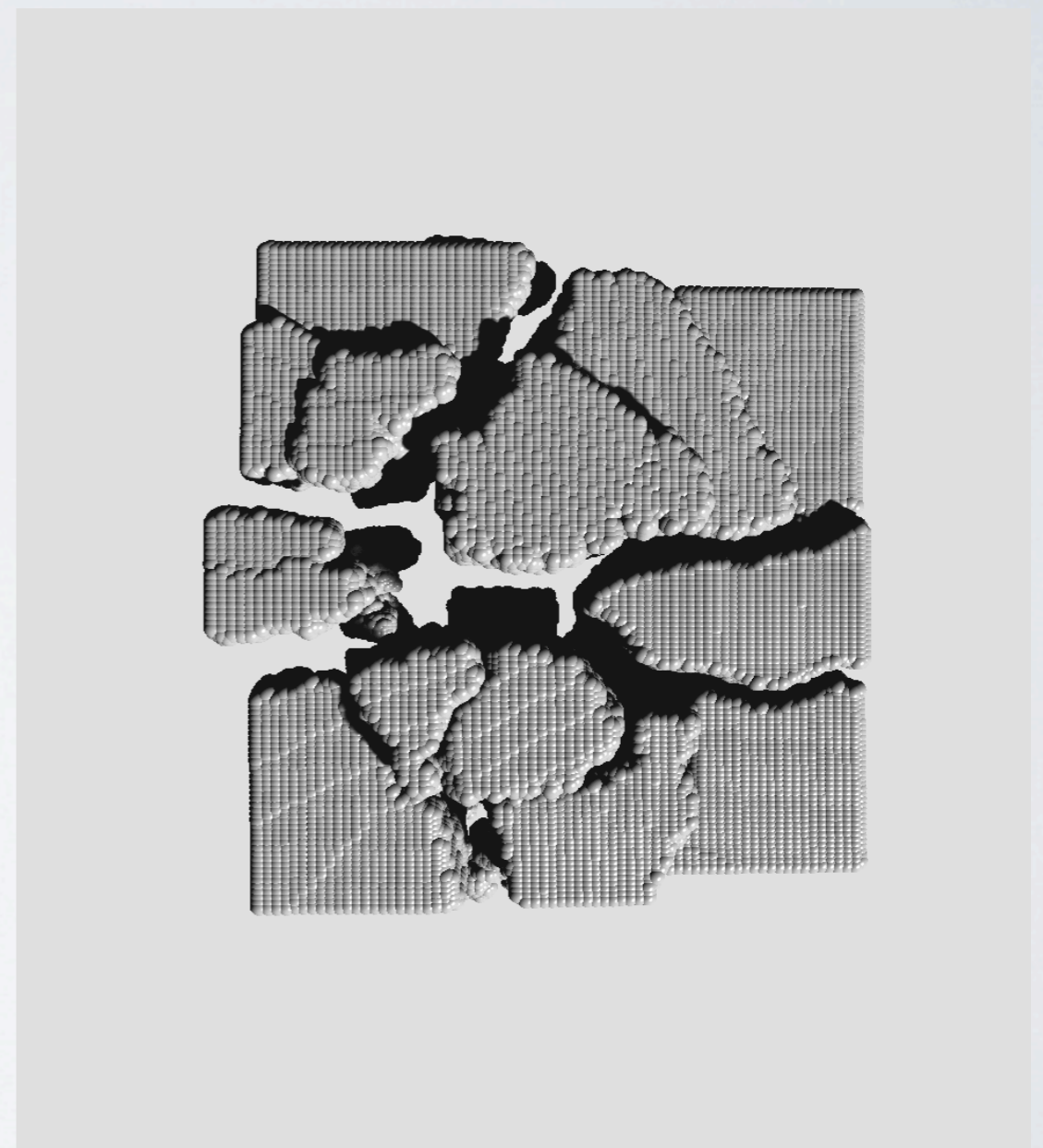
$t = 1.5 \text{ ms}$

Experiment



$V_{\text{antipodal}} = 5.9 \pm 1.6 \text{ m/s}$

Simulation (porous)



$V_{\text{antipodal}} = 5.6 \text{ m/s}$

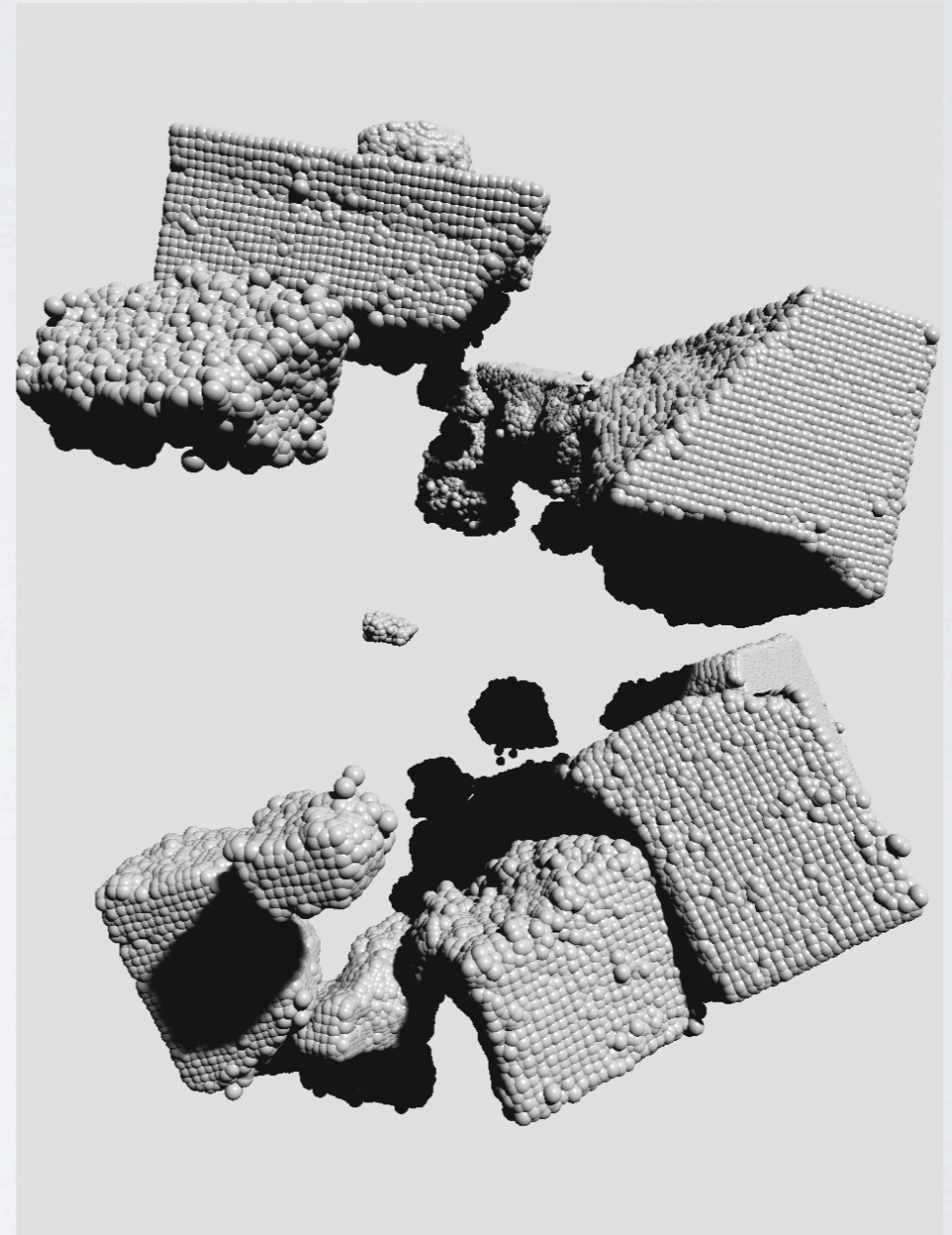
Comparison with laboratory experiments

$t = 8.0 \text{ ms}$

Experiment

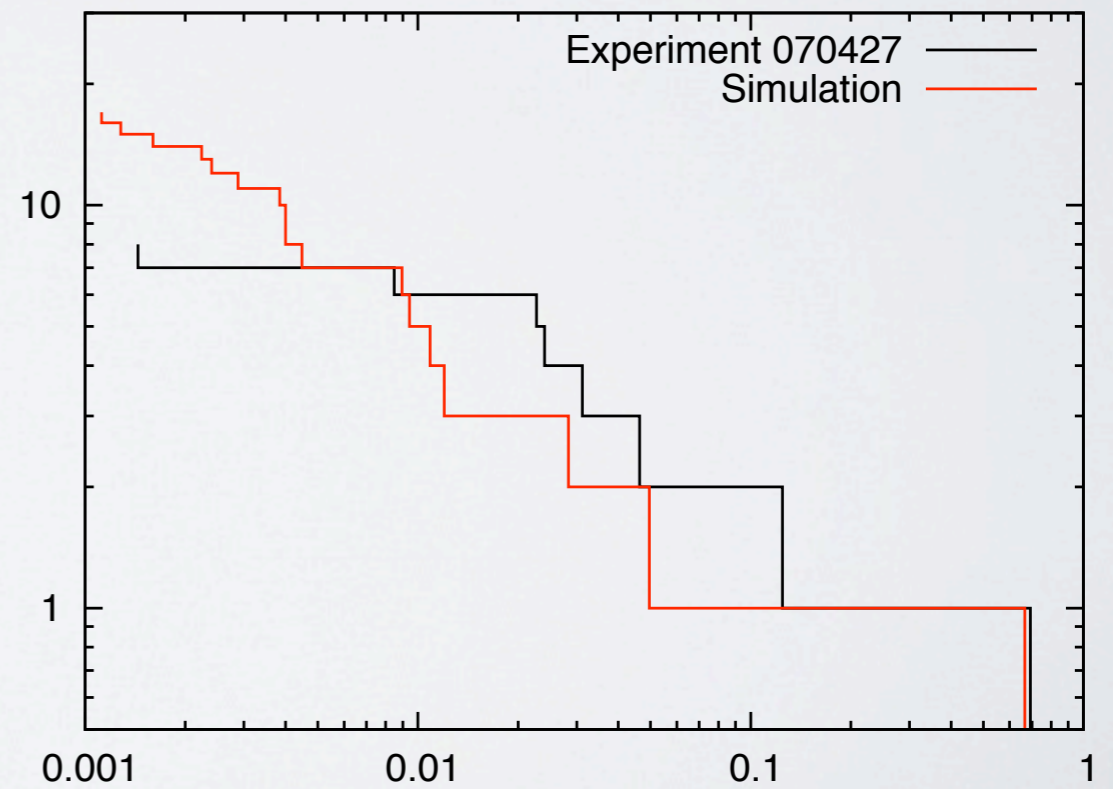
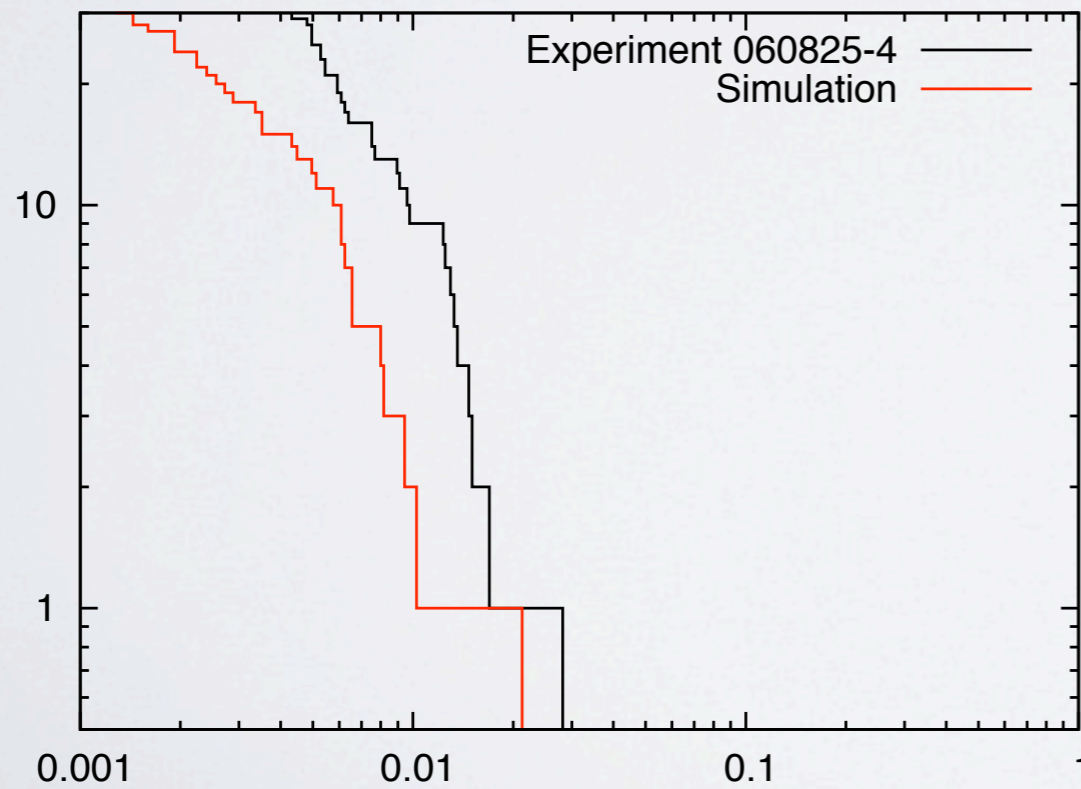
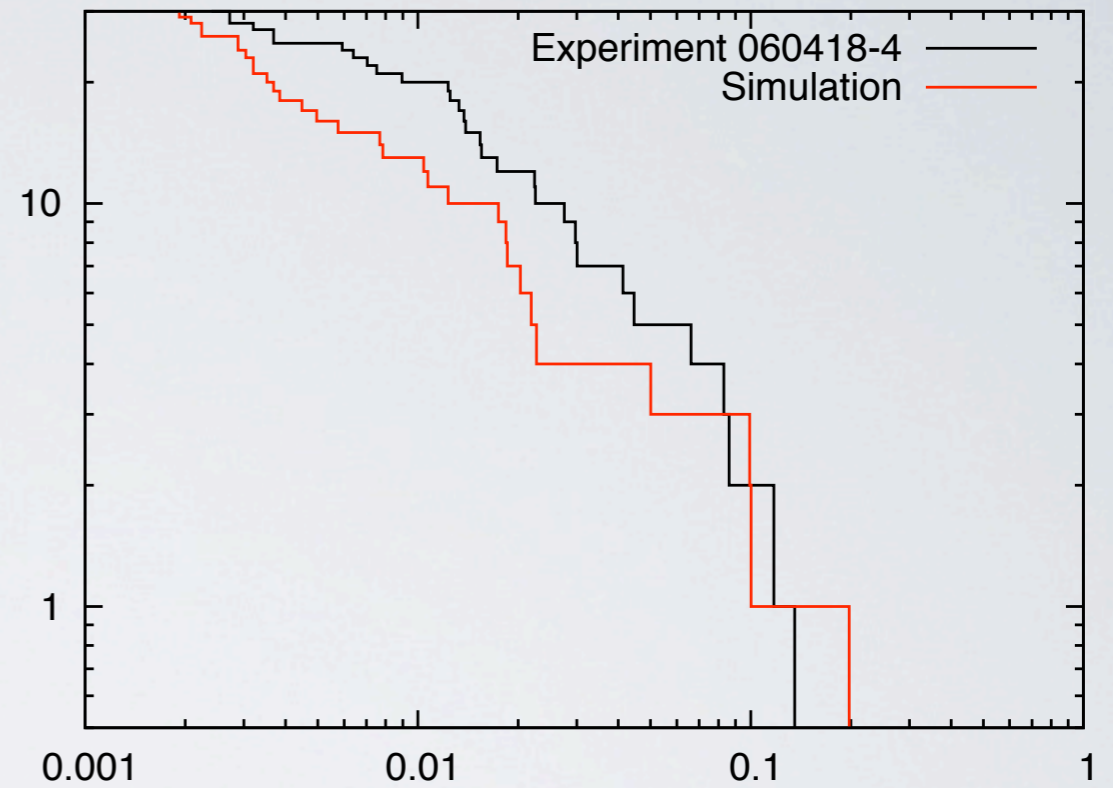
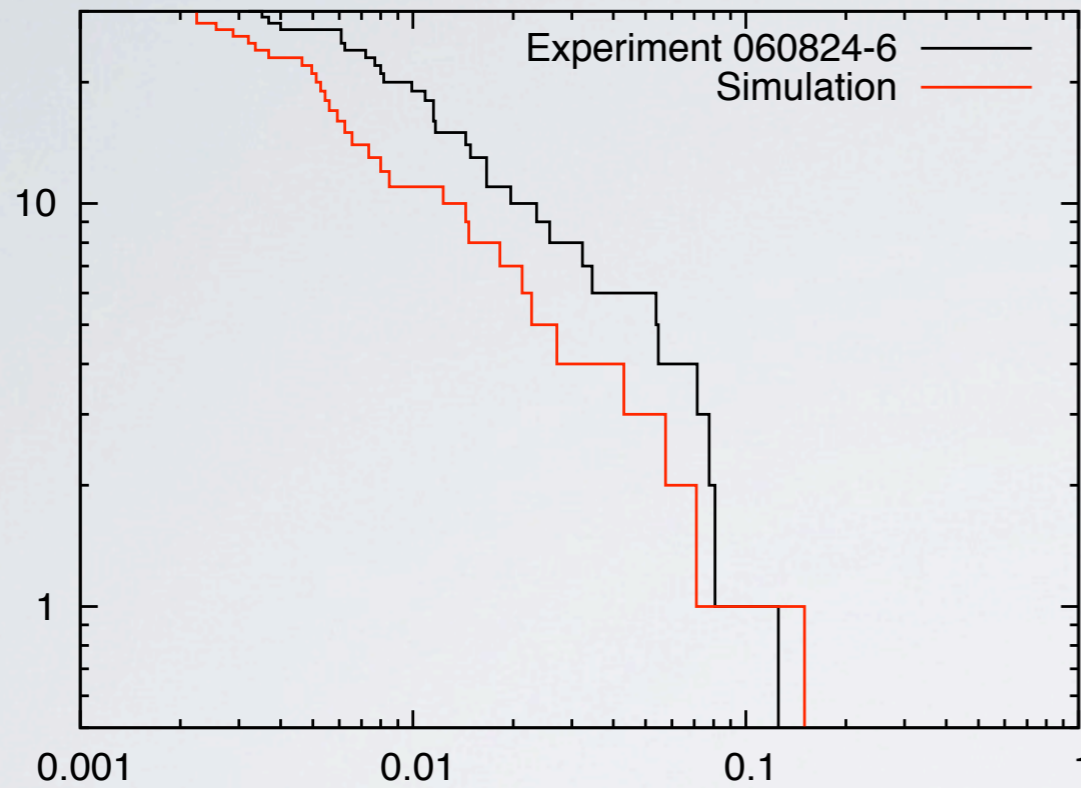


Simulation (porous)



Cumulative mass distribution

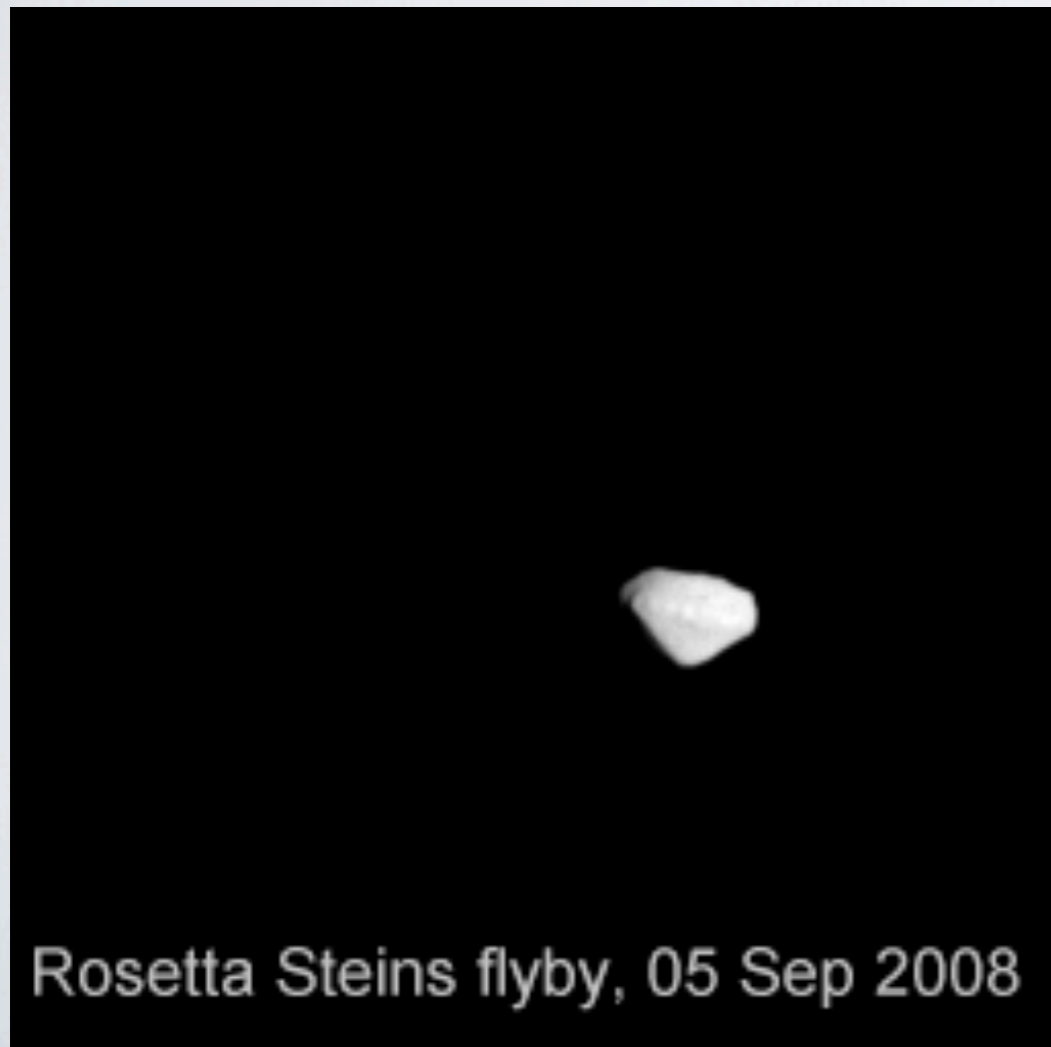
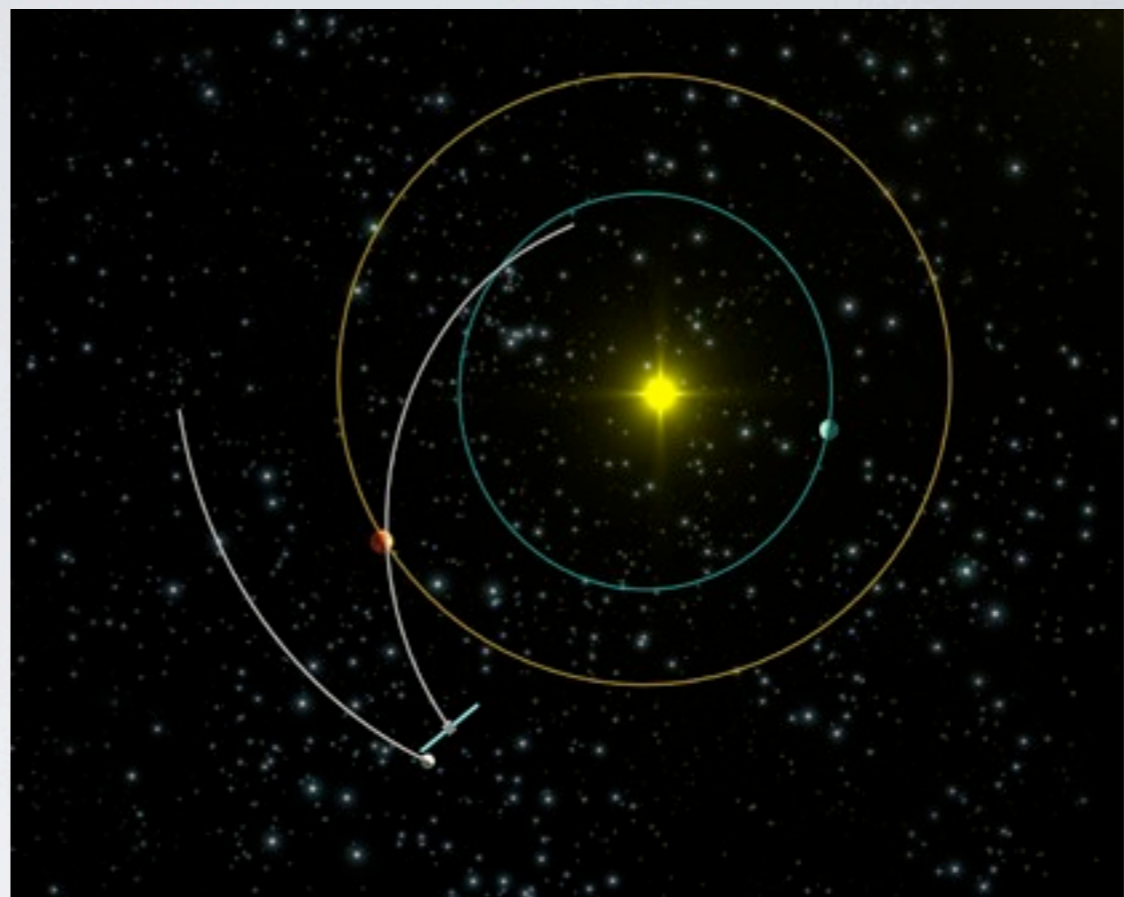
Cumulative number of fragments



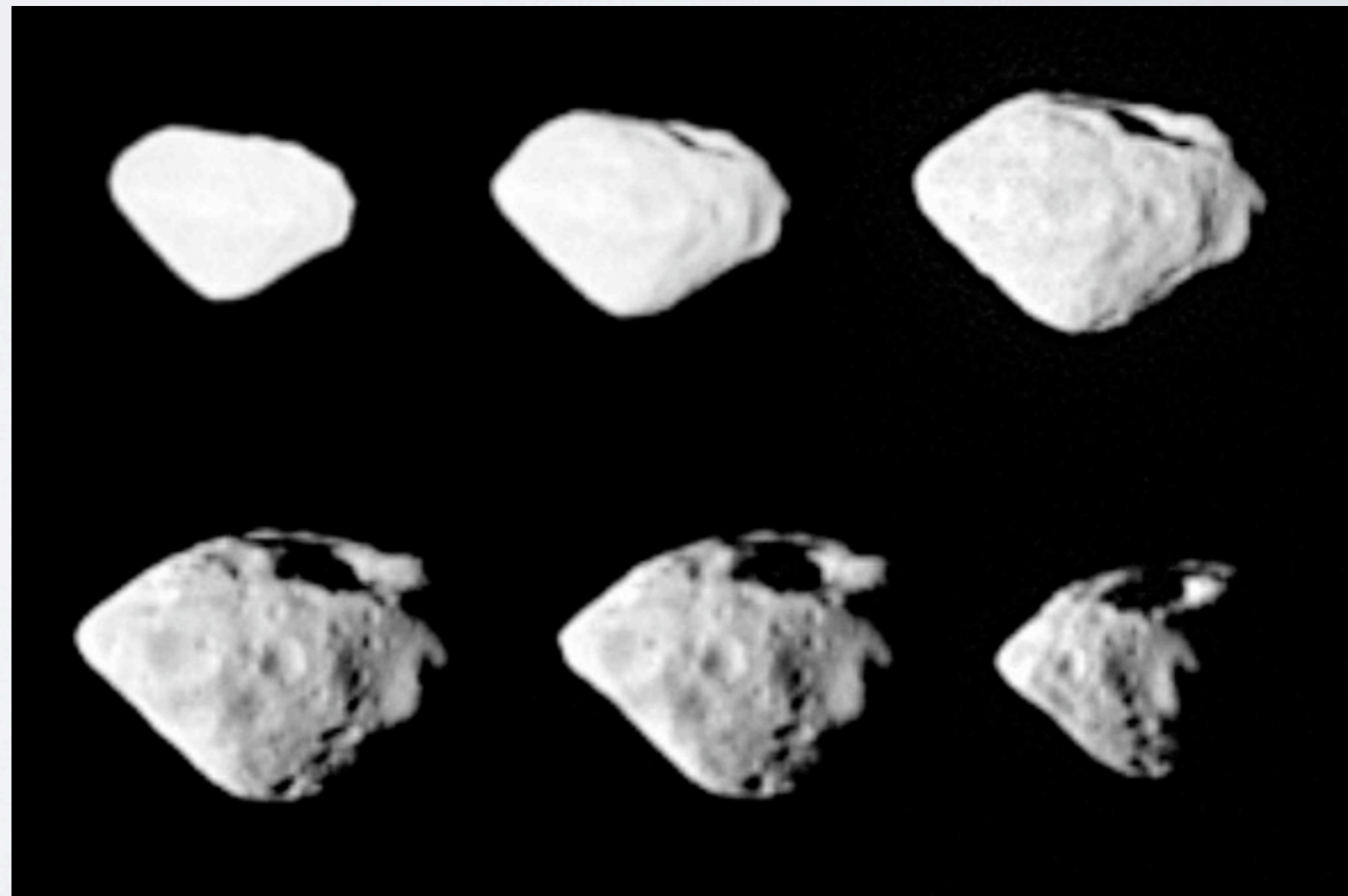
Mass fraction

Asteroid Steins

*Rosetta Fly-by
on 5 September 2008*



Rosetta Steins flyby, 05 Sep 2008



Asteroid Steins

What kind of impact produces such a crater?

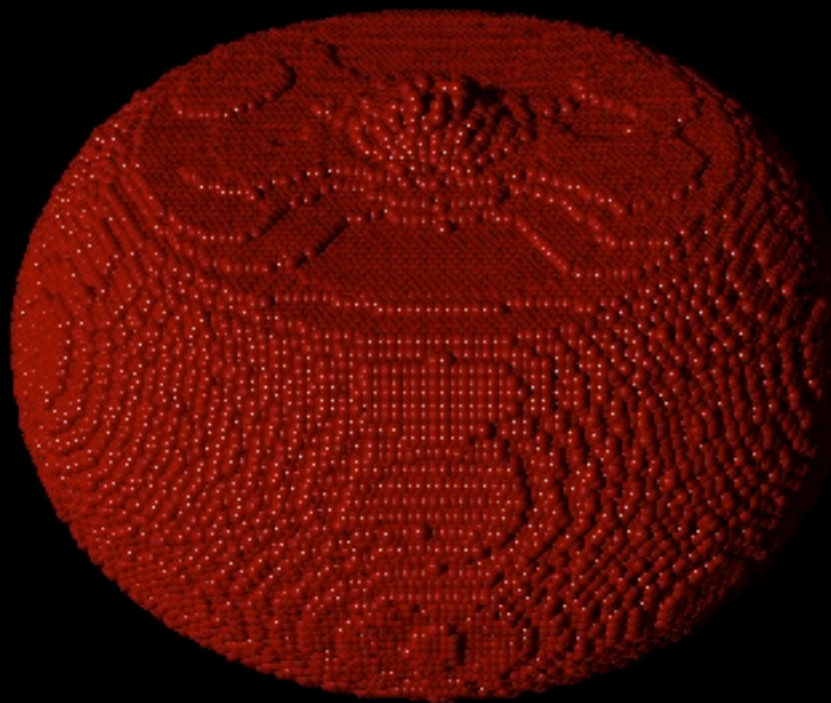


5.73 × 4.95 × 4.58 km

Impactor:

$D = 180 \text{ m}$

$V_{\text{imp}} = 5 \text{ km/s}$

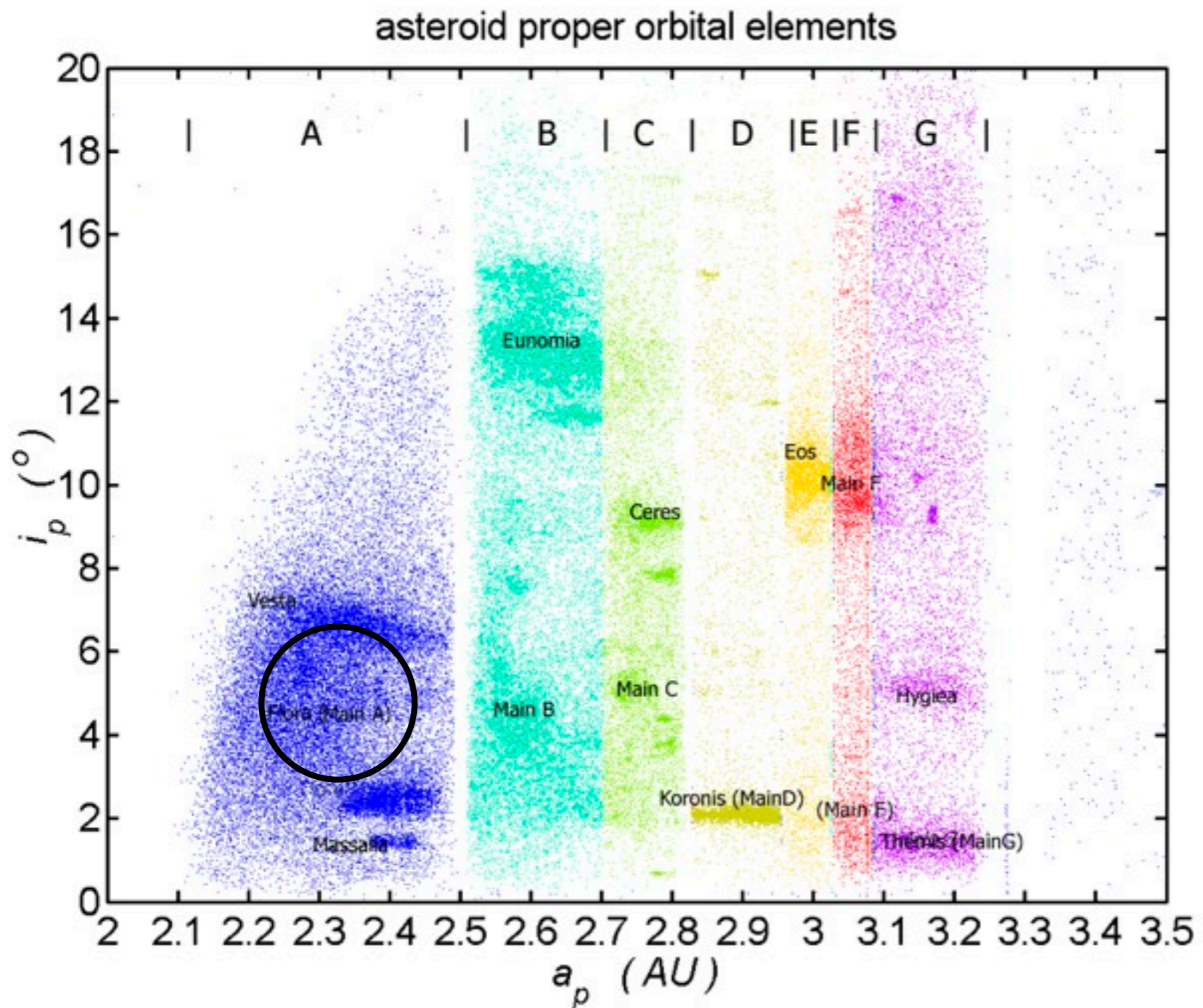


non-porous



porous
(25 % porosity)

Asteroid families: Evidences for disruptive collisions



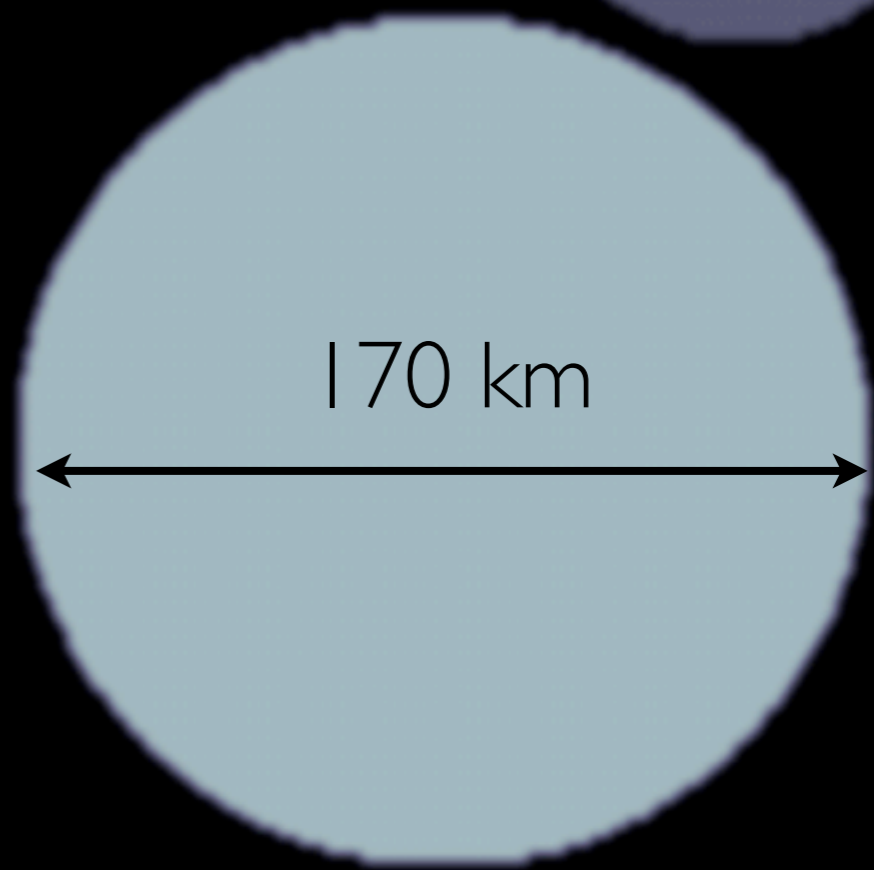
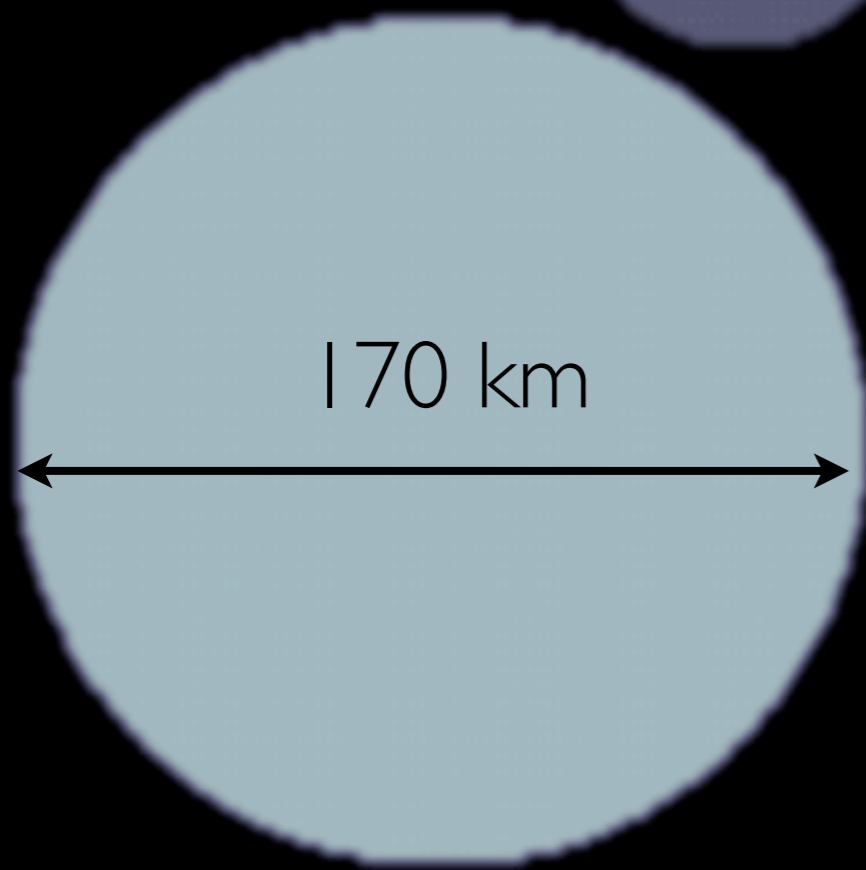
*asteroid families
provide the laboratory
to test codes in the
gravitational regime*

Disruptive collisions (at 3km/s)

Porous

Simulation: $t = 0 - 200 \text{ s}$

Non-Porous



Families: Disruption and re-accumulation

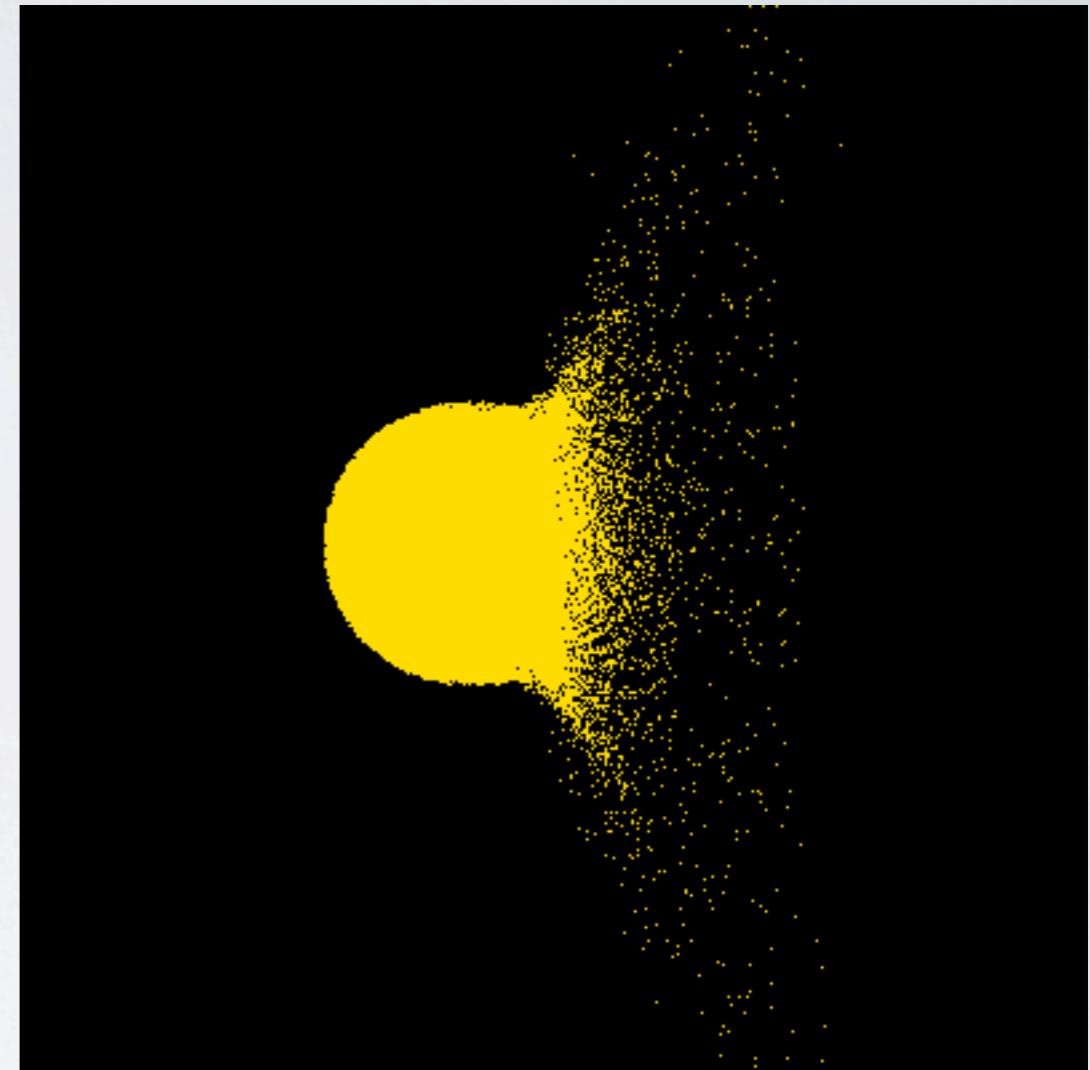
Flora family: Parent body 164 km

- 1) the parent body is totally disrupted by a catastrophic impact

SPH simulations

- 2) expanding debris are re-accumulating to form family members

Collisional N-body simulations



Explain the rubble pile nature of the larger objects



Conclusions

- 1) Collisions are at the heart of the evolution of the small bodies in the solar system
 - 2) The Lagrangian nature of SPH makes it an ideal tool to simulate impacts and collisions
 - 3) Material parameters play a key role in the modeling
 - can/should be measured in laboratory experiments
 - are not known for most of the bodies.
- *inverse problem: Use collisions to probe the material properties...*