

The finite volume particle method for flows with moving walls

Nathan J. Quinlan

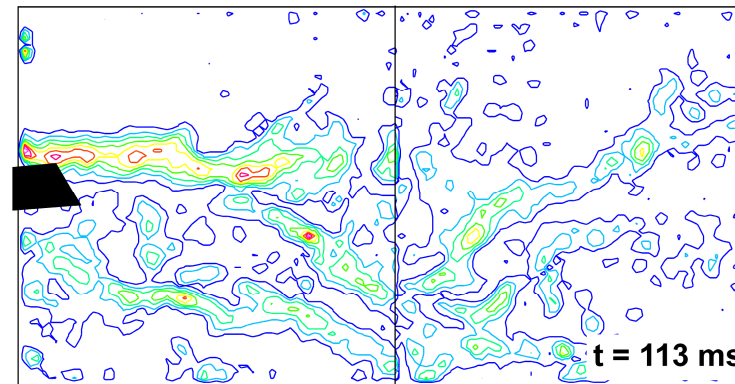
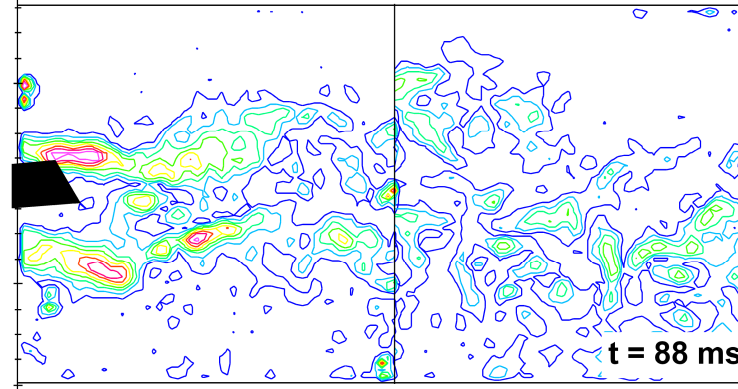
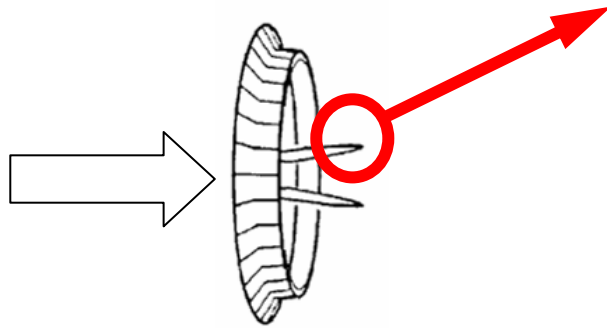
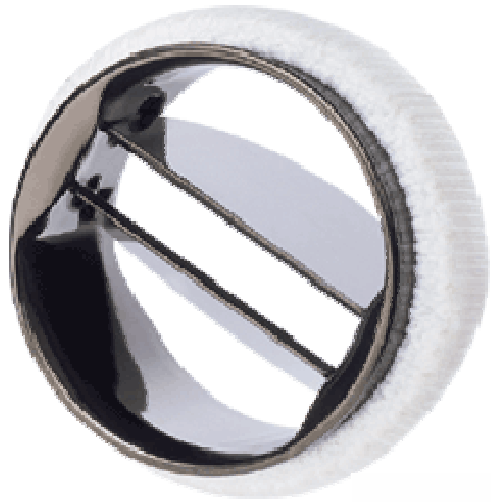
Mechanical and Biomedical Engineering
National University of Ireland, Galway

5th SPHERIC workshop
Manchester, 2010



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Motivation: biomedical fluid dynamics



Bellofiore et al., 2010

Mechanical
heart valve

$Re \cong 6000$



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The lineage of FVPM

Hietel, Steiner, Struckmeier 2000 *A finite-volume particle method for compressible flows*
2D, 1st order

Junk 2001 *Do finite volume methods need a mesh?*

Ismagilov 2005 Smooth volume integral method
1D with MUSCL

Keck, Hietel 2005 Incompressible flow

Nestor *et al.* 2008 2D with MUSCL, viscous flows

Nestor, Quinlan 2009 Incompressible, moving body



The finite volume particle method

Conservation law:
$$\frac{\partial \mathbf{U}}{\partial t} + \nabla \cdot \mathbf{F}(\mathbf{U}) = 0$$

Introduce a **compactly supported** test function $\psi_i(\mathbf{x})$:

weak form:
$$\int_{\Omega} \psi_i \frac{\partial \mathbf{U}}{\partial t} d\mathbf{x} + \int_{\Omega} \psi_i \nabla \cdot \mathbf{F}(\mathbf{U}) d\mathbf{x} = 0$$

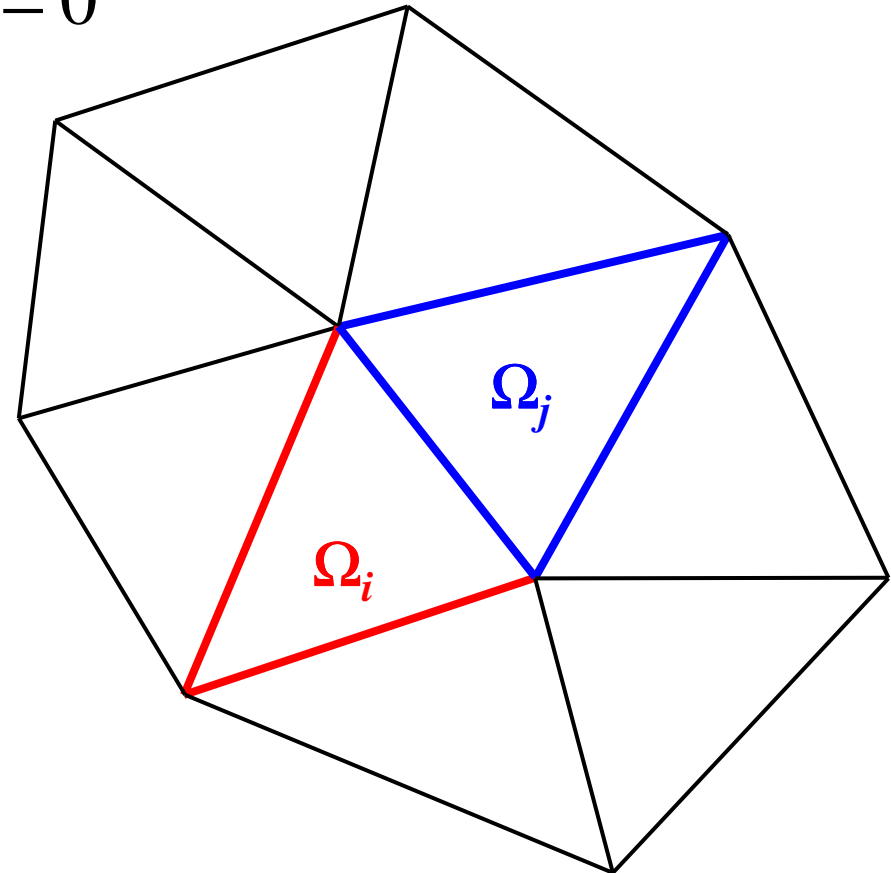
$$\int_{\Omega} \psi_i \frac{\partial \mathbf{U}}{\partial t} d\mathbf{x} - \int_{\Omega} \nabla \psi_i \cdot \mathbf{F}(\mathbf{U}) d\mathbf{x} = 0$$



Choice of test function and support volume

$$\int_{\Omega} \psi_i \frac{\partial \mathbf{U}}{\partial t} d\mathbf{x} - \int_{\Omega} \nabla \psi_i \cdot \mathbf{F}(\mathbf{U}) d\mathbf{x} = 0$$

$$\psi_i(\mathbf{x}) = \begin{cases} 1 & x \in \Omega_i \\ 0 & \text{otherwise} \end{cases}$$



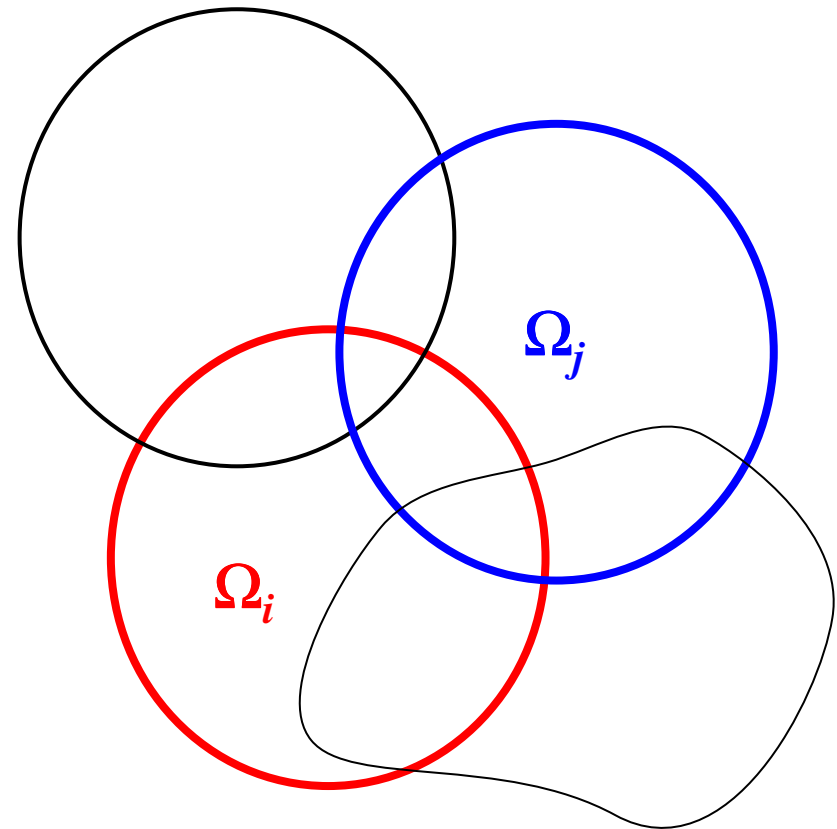
→ finite volume method

Choice of test function and support volume

$$\int_{\Omega} \psi_i \frac{\partial \mathbf{U}}{\partial t} d\mathbf{x} - \int_{\Omega} \nabla \psi_i \cdot \mathbf{F}(\mathbf{U}) d\mathbf{x} = 0$$

$$\psi_i(\mathbf{x}) = \frac{W_i(\mathbf{x})}{\sum_k W_k(\mathbf{x})}$$

where $W_i(\mathbf{x}) = 0$ for $x \notin \Omega_i$



FVPM

→ finite volume **particle** method

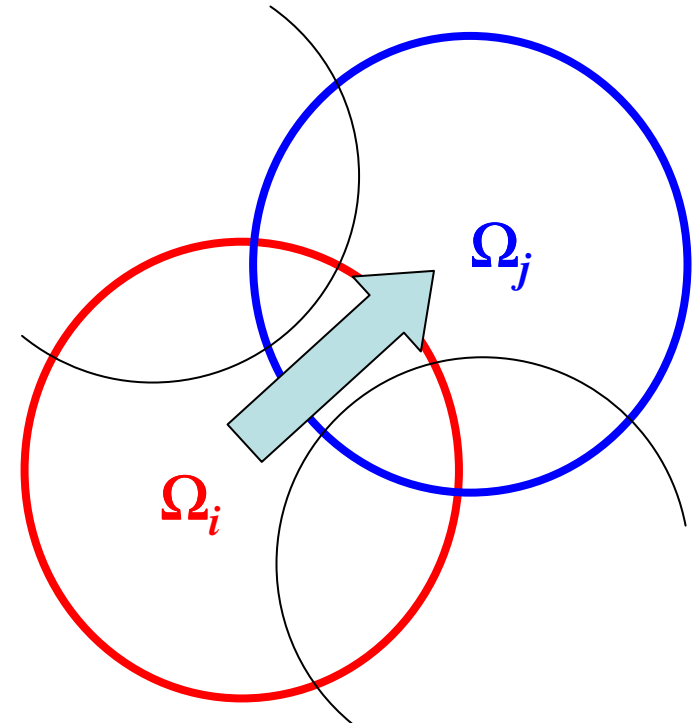


Interpretation in terms of pair interactions

$$\int_{\Omega} \psi_i \frac{\partial \mathbf{U}}{\partial t} d\mathbf{x} - \int_{\Omega} \nabla \psi_i \cdot \mathbf{F}(\mathbf{U}) d\mathbf{x} = 0$$

$$\sum_j \frac{W_i(\mathbf{x}) \nabla W_j(\mathbf{x}) - W_j(\mathbf{x}) \nabla W_i(\mathbf{x})}{\left(\sum_k W_k(\mathbf{x}) \right)^2}$$

$$\int_{\Omega} \psi_i \frac{\partial \mathbf{U}}{\partial t} d\mathbf{x} - \sum_j \int_{\Omega} (\gamma_{ij} - \gamma_{ji}) \cdot \mathbf{F}(\mathbf{U}) d\mathbf{x} = 0$$



3 approximations in FVPM, as in finite volume

$$\frac{d}{dt} \int_{\Omega} \psi_i \mathbf{U} d\mathbf{x} - \sum_j \int_{\Omega} (\gamma_{ij} - \gamma_{ji}) \cdot \mathbf{F}(\mathbf{U}) d\mathbf{x} - \int_{\Omega} \frac{\partial \psi_i}{\partial t} \mathbf{U} d\mathbf{x} = 0$$

1 Replace the weighted volume average of \mathbf{U} with a "particle" value

2 Represent $\mathbf{F}(\mathbf{U}(\mathbf{x}, t))$ with a single value for the overlap region

$$\frac{d}{dt} (V_i \mathbf{U}_i) - \sum_j \beta_{ij} \mathbf{F}_{ij} - \int_{\Omega} \frac{d\psi_i}{dt} \mathbf{U} d\mathbf{x} = 0$$

where

$$V_i = \int_{\Omega} \psi_i d\mathbf{x}$$

Reconstruct $\mathbf{U}_i, \mathbf{U}_j$ at interface for Riemann problem

3

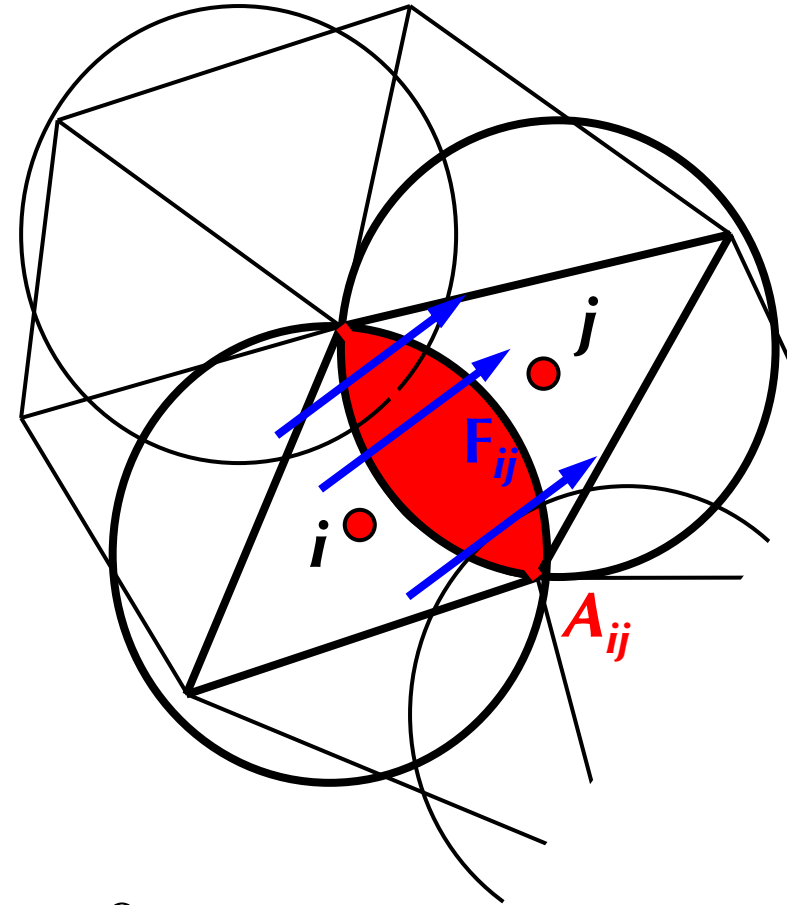
$$\rightarrow \mathbf{F}_{ij} \cong \mathbf{F}(\mathbf{U}_i, \mathbf{U}_j)$$

Analogy with mesh finite volume method

FVM

$$\frac{d}{dt}(V_i \mathbf{U}_i) - \sum_j \mathbf{A}_{ij} \cdot (\mathbf{F}_{ij} + \dot{\mathbf{x}}_{ij} \mathbf{U}_{ij}) = 0$$

$$\mathbf{A}_{ij} \longleftrightarrow \beta_{ij}$$



FVPM

$$\frac{d}{dt}(V_i \mathbf{U}_i) - \sum_j \beta_{ij} \cdot (\mathbf{F}_{ij} + \dot{\mathbf{x}}_{ij} \mathbf{U}_{ij}) = 0$$



The particle interaction vector

$$\beta_{ij} = \int \frac{W_i \nabla W_j - W_j \nabla W_i}{\left(\sum_k W_k(\mathbf{x}) \right)^2} d\mathbf{x}$$

$W(\mathbf{x})$ is any kernel with compact support

2 properties of β_{ij}

$\beta_{ij} = -\beta_{ji}$ symmetry \Rightarrow **exact conservation**

$\sum_j \beta_{ij} = 0$ the particle volume is “closed”
 \Rightarrow **zero-order consistency**

The mesh finite volume method is a special case of FVPM.

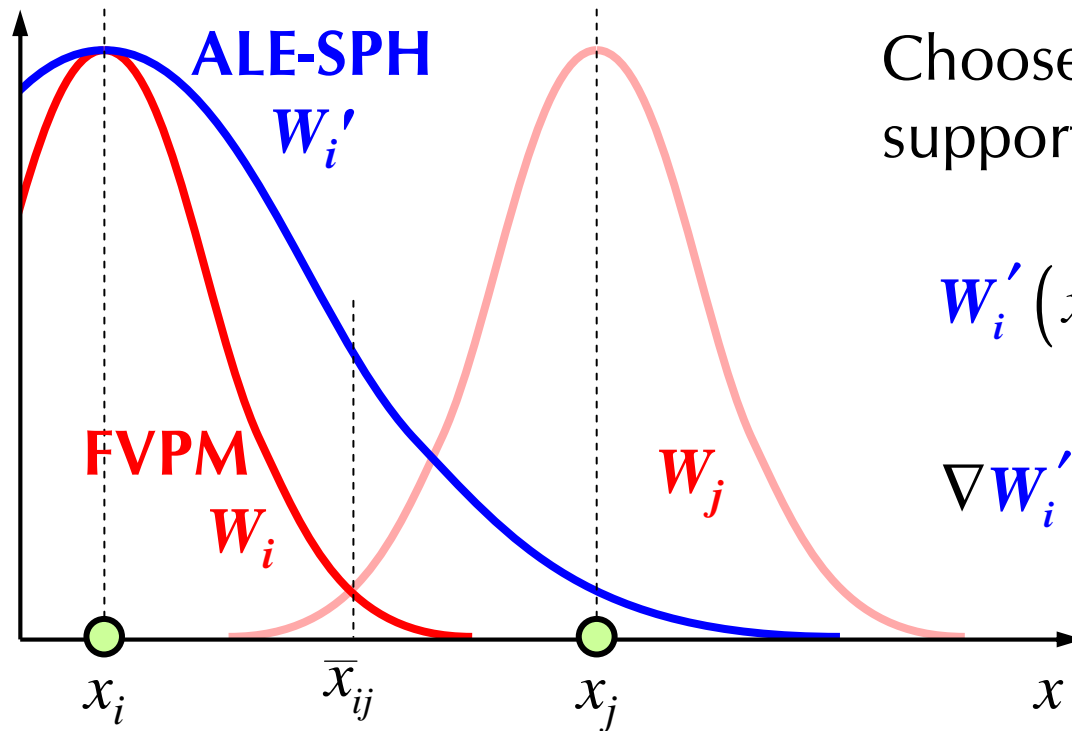
(Junk, 2003)



Relationship to ALE-SPH

$$\frac{d}{dt}(V_i \mathbf{U}_i) - 2V_i \sum_j V_j \mathbf{G}(\mathbf{U}_i, \mathbf{U}_j) \cdot \nabla \mathbf{W}'_i(\mathbf{x}_j) = 0$$

Vila (1999)



Choose \mathbf{W}' with double the support radius of $\mathbf{W} \Rightarrow$

$$\mathbf{W}'_i(x_j) = \mathbf{W}_i(x_{ij})$$

$$\nabla \mathbf{W}'_i(x_j) = \frac{1}{2} \nabla \mathbf{W}_i(x_{ij})$$



Relationship to ALE-SPH

Shepard-normalised RSPH kernel: $\tilde{W}'_i(\mathbf{x}) = \frac{W'_i(\mathbf{x})}{\sum_k W'_k(\mathbf{x}) V_k}$

Approximate relationship: $\nabla \tilde{W}'_i(x_j) \cong \frac{1}{2} \nabla \tilde{W}_i(x_{ij})$

$$\nabla \tilde{W}'_i(x_j) = \sum_j \left[\frac{W'_i \nabla W'_j - W'_j \nabla W'_i}{\left(\sum_k W'_k \right)^2 V} \right]_{x=x_j} \cong \frac{1}{2} \sum_j \left[\frac{W_i \nabla W_j - W_j \nabla W_i}{\left(\sum_k W_k \right)^2 V} \right]_{x=\bar{x}_{ij}}$$

(if $V_i = V_j = V$)



Relationship to ALE-SPH

ALE-SPH approximates

$$\frac{d}{dt}(V_i \mathbf{U}_i) - \sum_j \mathbf{G}(\mathbf{U}_i, \mathbf{U}_j) \cdot V_i \left[\frac{W_i \nabla W_j - W_j \nabla W_i}{\left(\sum_k W_k \right)^2} \right]_{x=\bar{x}_{ij}} = 0$$

FVPM is

$$\frac{d}{dt}(V_i \mathbf{U}_i) - \sum_j \mathbf{G}(\mathbf{U}_i, \mathbf{U}_j) \cdot \int_{\Omega_i \cap \Omega_j} \frac{W_i \nabla W_j - W_j \nabla W_i}{\left(\sum_k W_k \right)^2} d\mathbf{x} = 0$$

overlap volume \cong material volume

\Rightarrow **RSPH \cong FVPM with a single-point approximation to β_{ij}**



A continuum from SPH to finite volume?

$$\text{SPH} \quad -\left(\frac{p_i}{\rho_i^2} + \frac{p_j}{\rho_j^2}\right) \nabla W_{ij} V_j$$

$$\text{ALE-SPH} \quad -2V_i V_j \nabla W_{ij} \mathbf{F}(\mathbf{U}_i, \mathbf{U}_j)$$

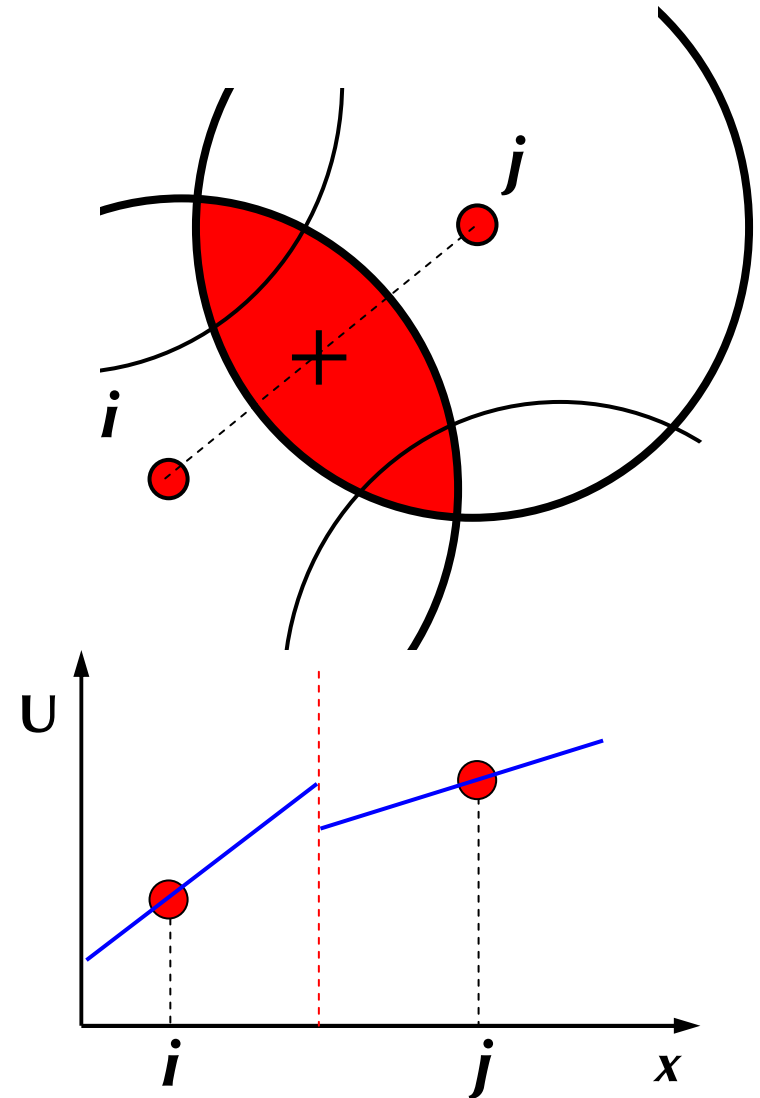
$$\text{FVPM} \quad -\beta_{ij} \mathbf{F}(\mathbf{U}_i, \mathbf{U}_j)$$

$$\text{finite volume} \quad -\mathbf{A}_{ij} \mathbf{F}(\mathbf{U}_i, \mathbf{U}_j)$$

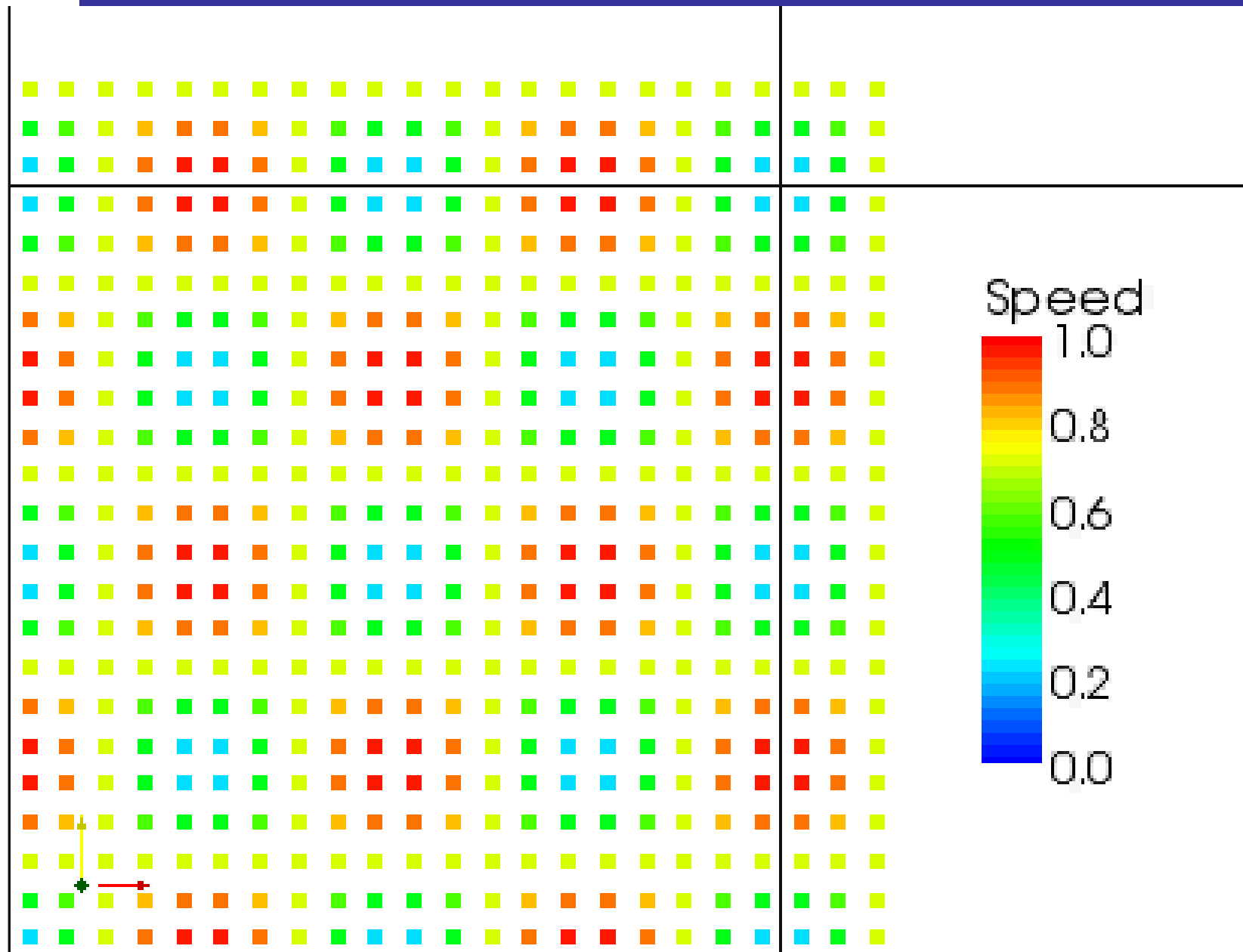


Higher-order spatial accuracy by MUSCL

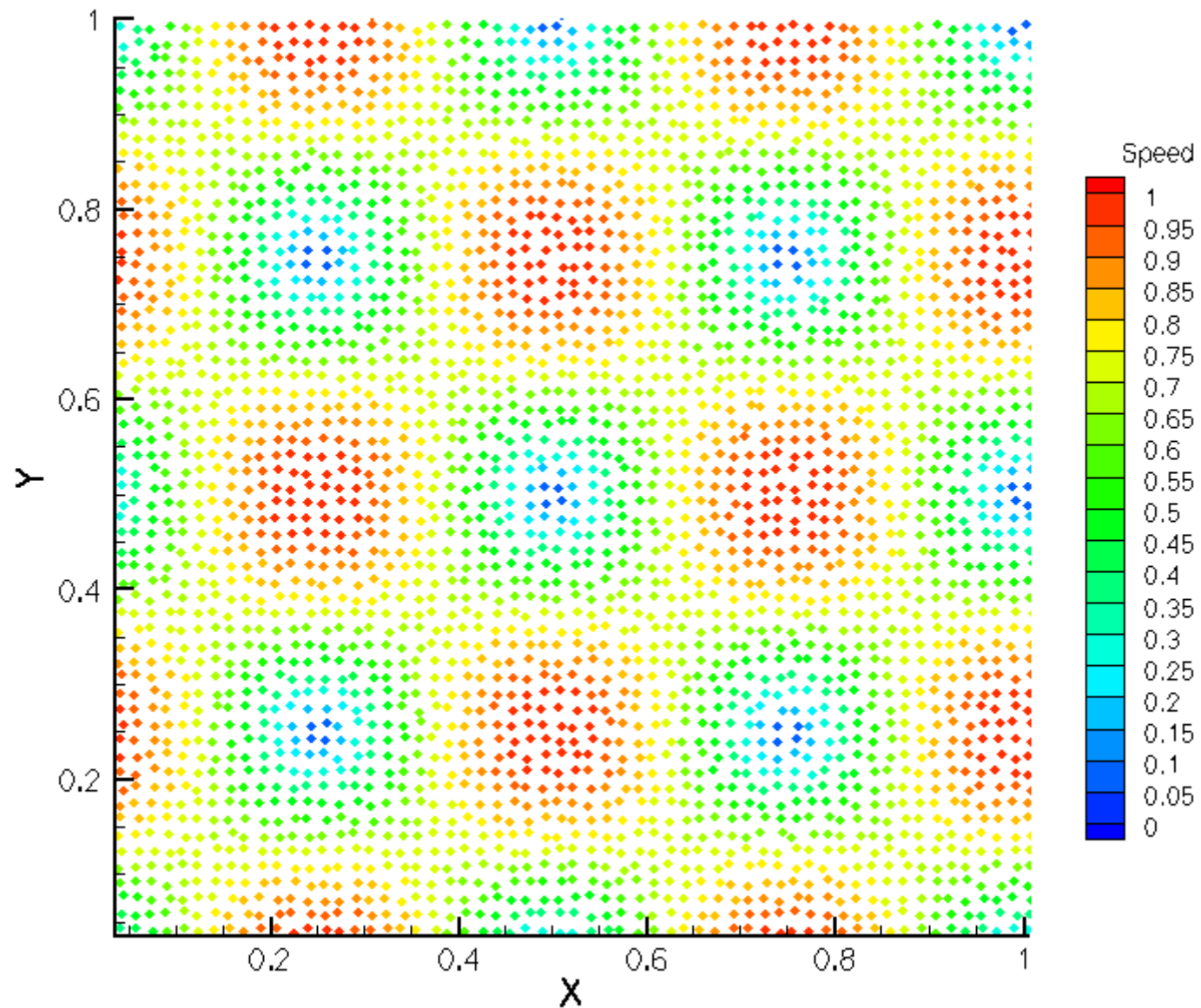
- Evaluate gradients at particle barycentres using (corrected) SPH approximation
- Reconstruct U_L and U_R on both sides of interface
- Compute approximate numerical flux $F(U_L, U_R)$



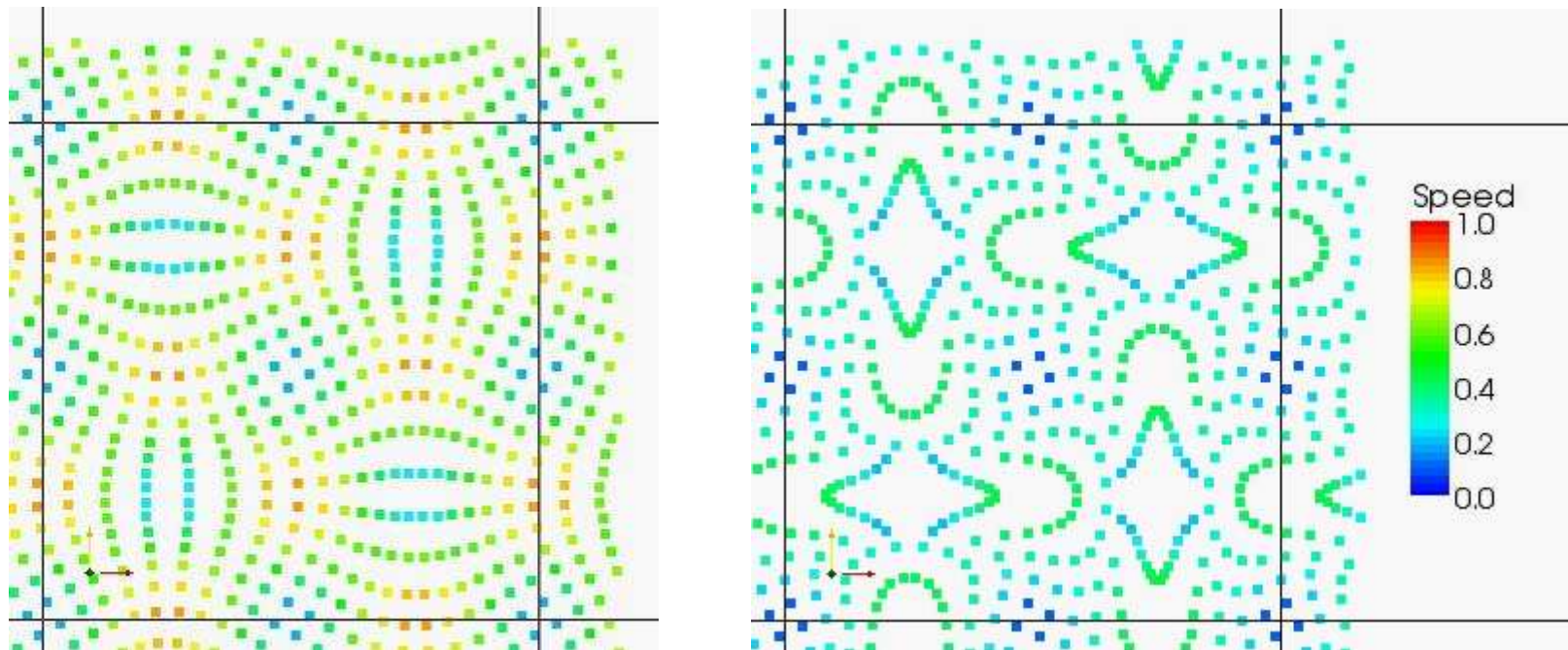
Taylor-Green flow at $Re = 100$, Lagrangian



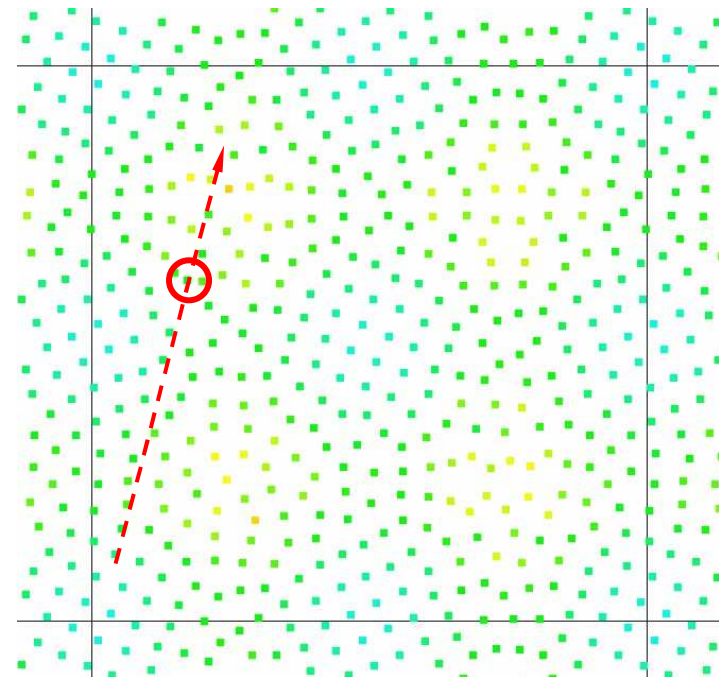
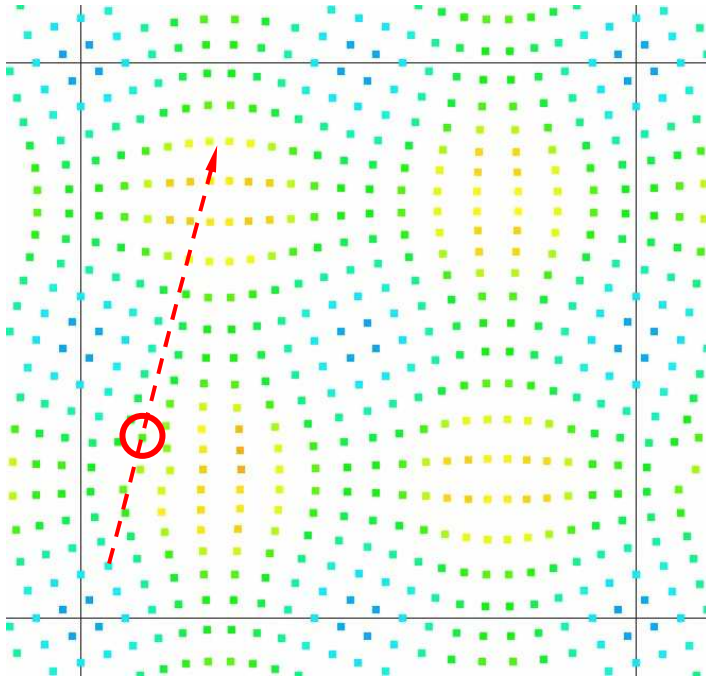
Randomised initialisation, Lagrangian



Taylor-Green, $Re = 100$, corrected Lagrangian

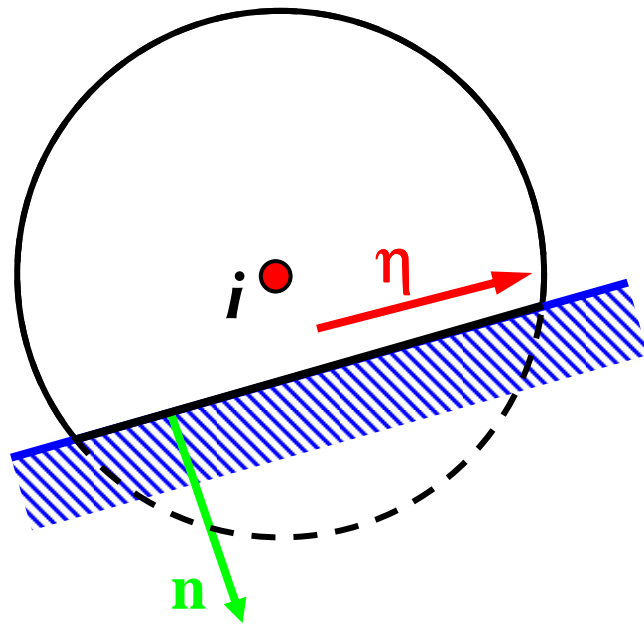


Taylor-Green flow with rogue particle



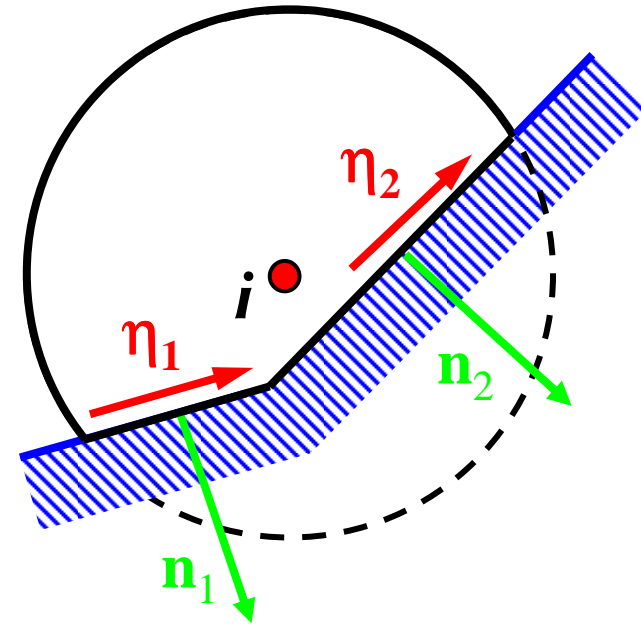
Boundary conditions

Particle support is truncated at boundary.



Compute boundary interaction vector directly...

$$\beta_i^b = \int \frac{W_i}{\sum_k W_k(\mathbf{x})} \mathbf{n} d\eta$$

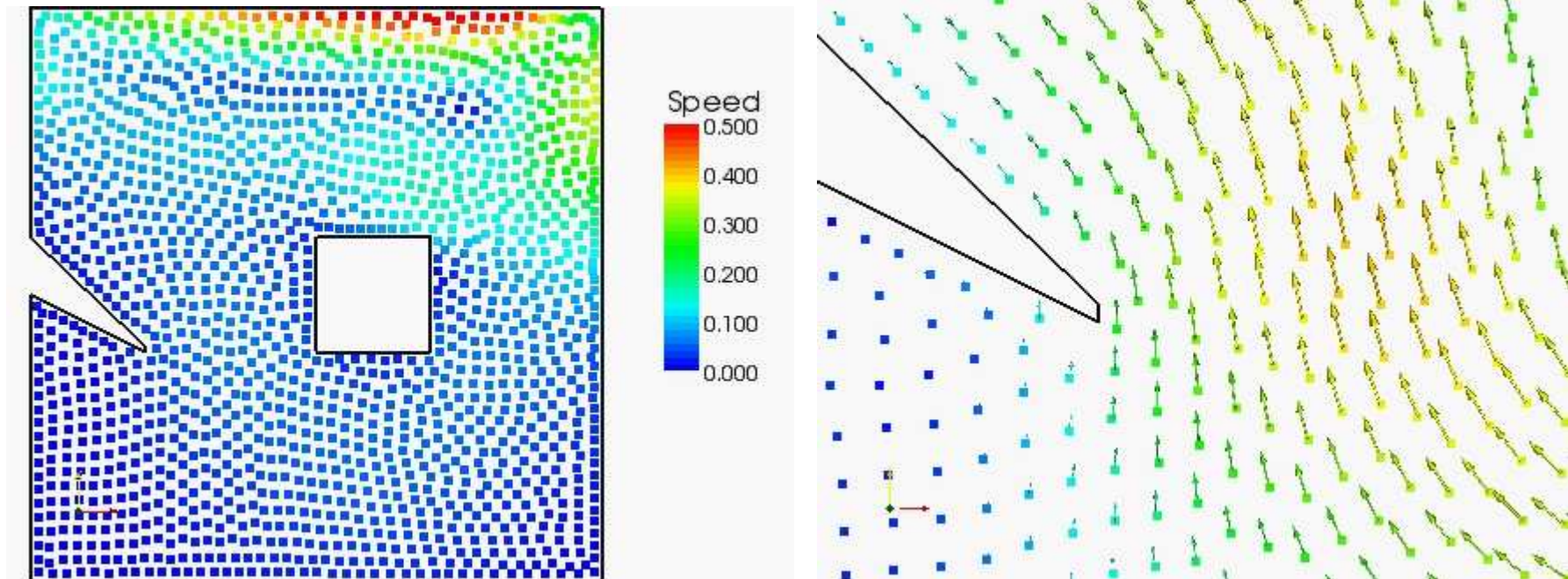


...or by enforcing

$$\sum_j \beta_{ij} + \beta_i^b = 0$$

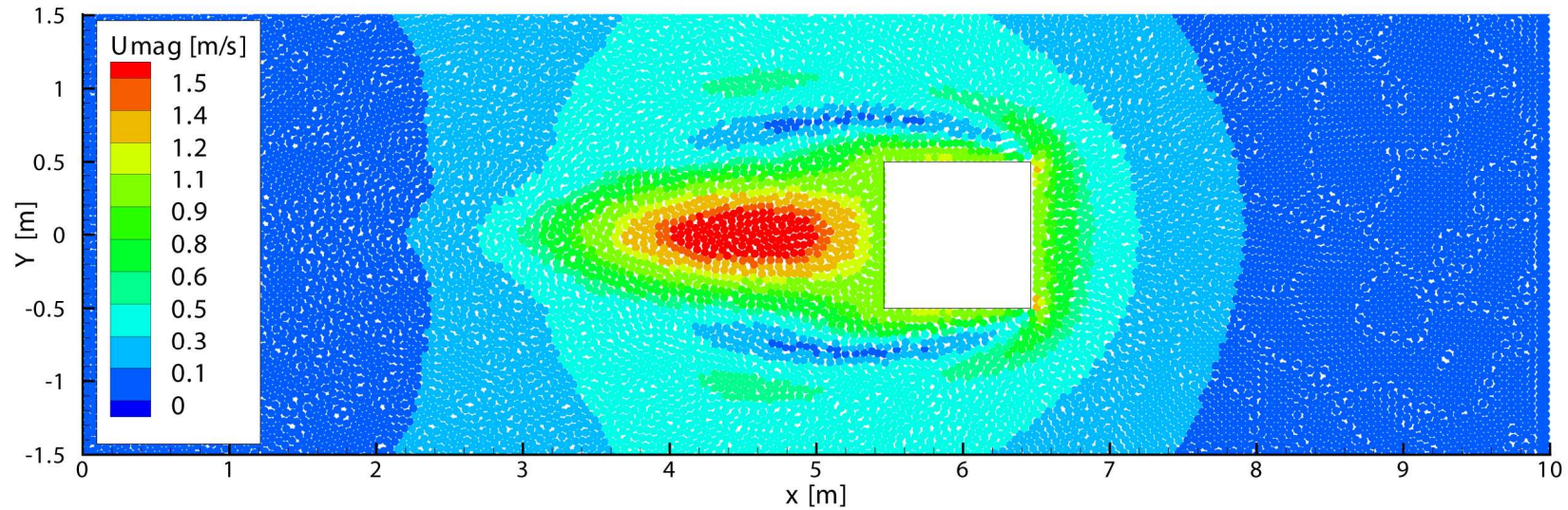


“Complex” geometry – $Re_L=100$

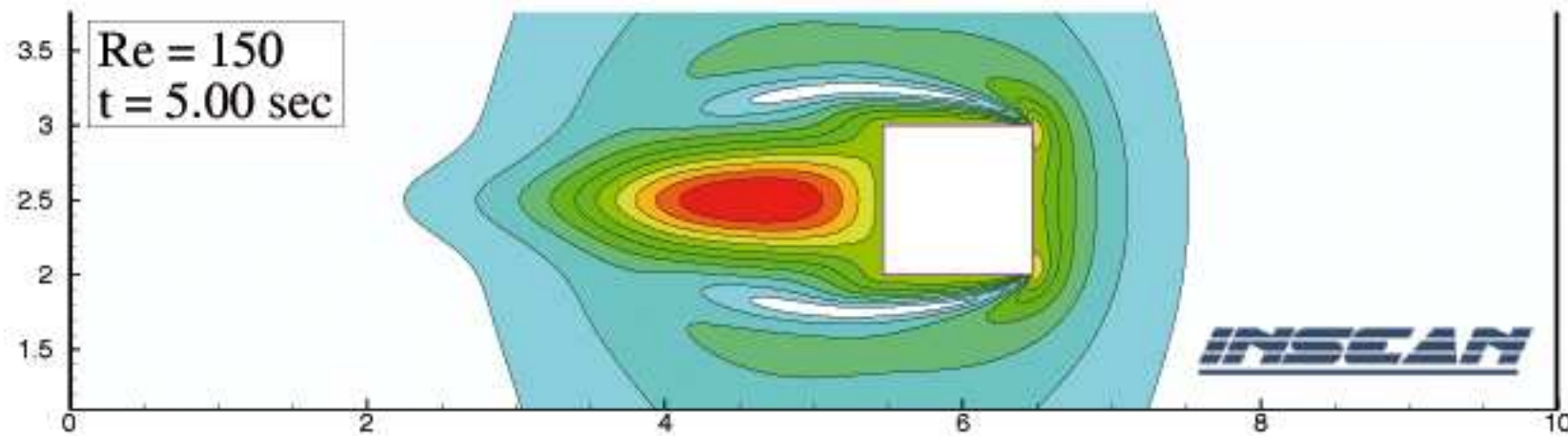


SPHERIC benchmark 6: moving square

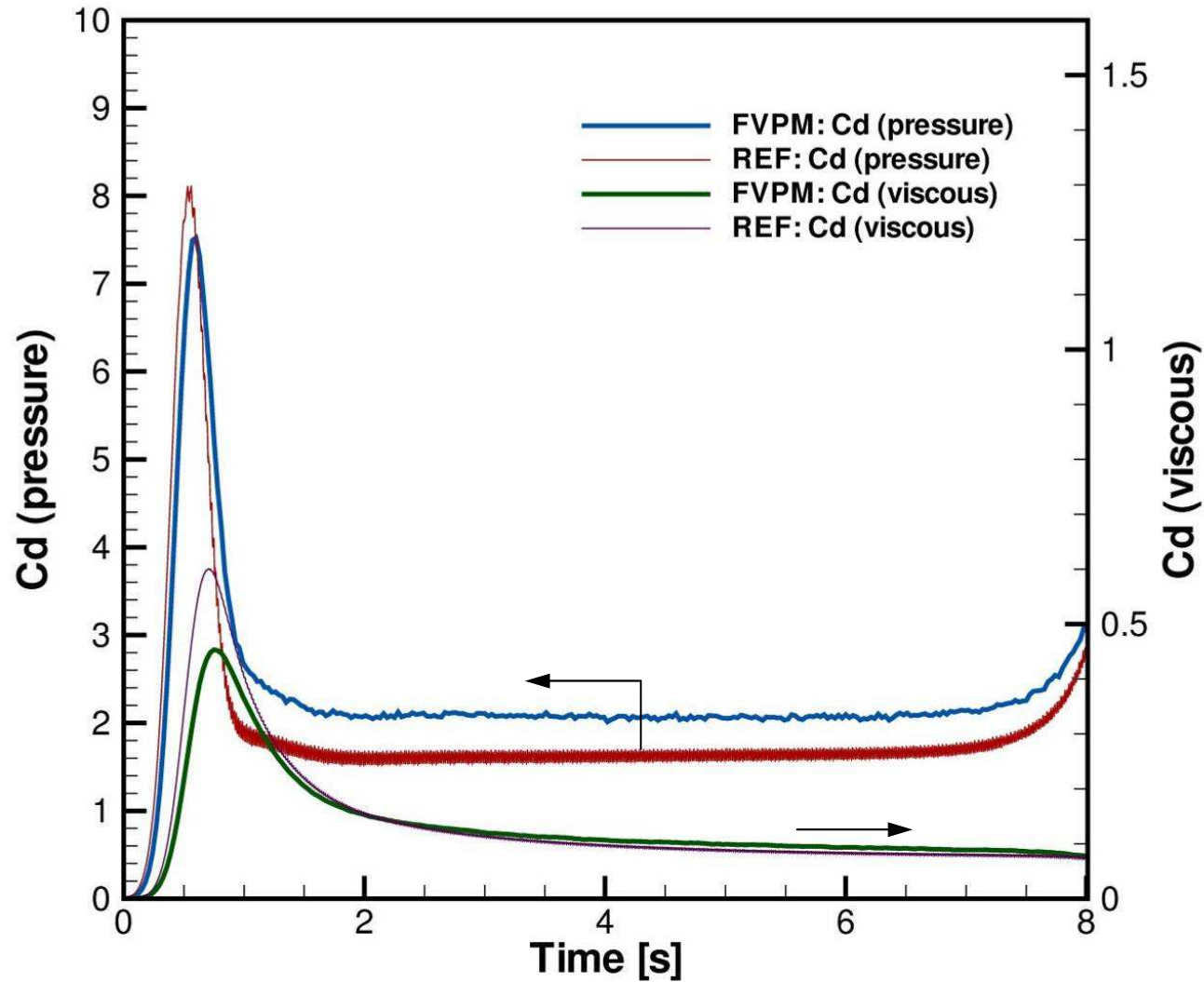
FVPM



Level set (Colagrossi)



SPHERIC benchmark 6: moving square

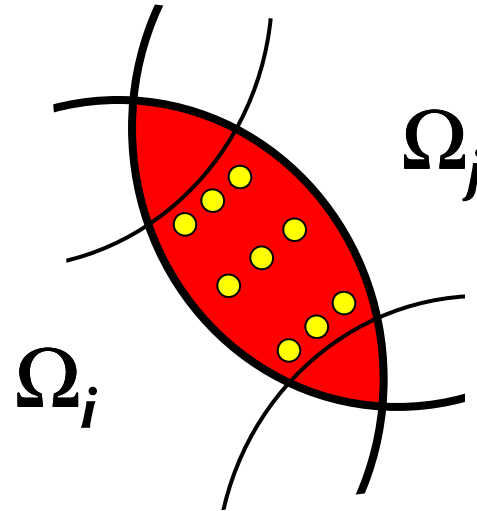


Correction of numerical β_{ij}

$$\beta_{ij} = \int \frac{W_i \nabla W_j - W_j \nabla W_i}{\left(\sum_k W_k(\mathbf{x}) \right)^2} d\mathbf{x}$$

Numerical integration is necessary.

Typically 6×6 quadrature points.



Correction options

Self-flux (Teleaga and Struckmeier, 2008)

- Preserves uniform states
- violates conservation

Pairwise shifting (Hietel and Keck, 2003)

- Restores conservation
- Errors are shifted to neighbouring particles



Computation time

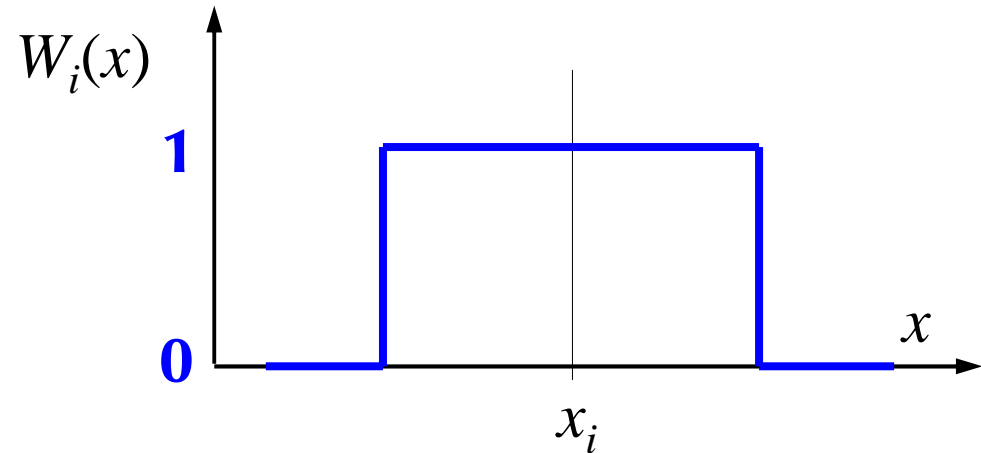
neighbour search	< 1%
flux	4%
gradients	2%
particle update	2%
motion correction	< 1%
β_{ij}	74%
barycentres	14%



Exact (and fast) evaluation of β_{ij}

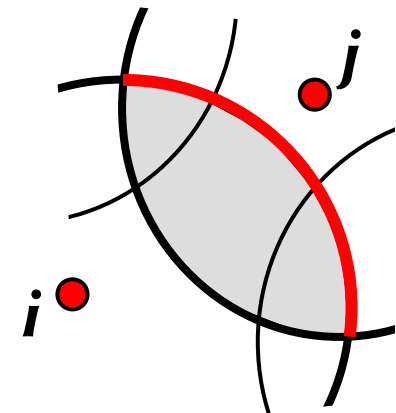
Choose the simplest possible kernel

$$W_i(x) = \begin{cases} 1 & x \in \Omega_i \\ 0 & \text{otherwise} \end{cases}$$



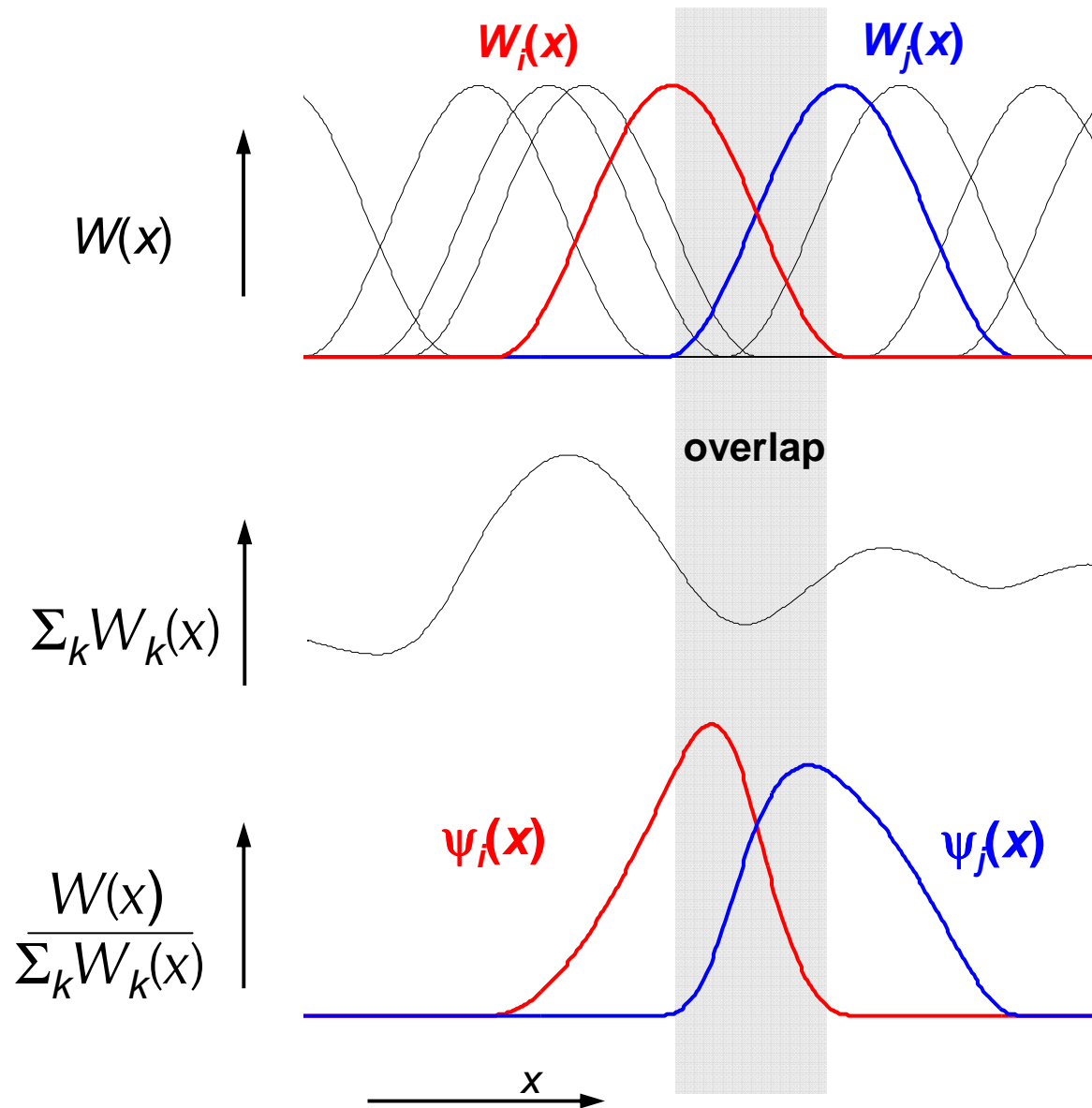
$$\beta_{ij} = \int \frac{W_i \nabla W_j - W_j \nabla W_i}{\left(\sum_k W_k(\mathbf{x}) \right)^2} d\mathbf{x}$$

$\nabla W_i = 0$ everywhere except on boundary of i



Integration over $\Omega_i \cap \Omega_j$ reduces to integration along a curve

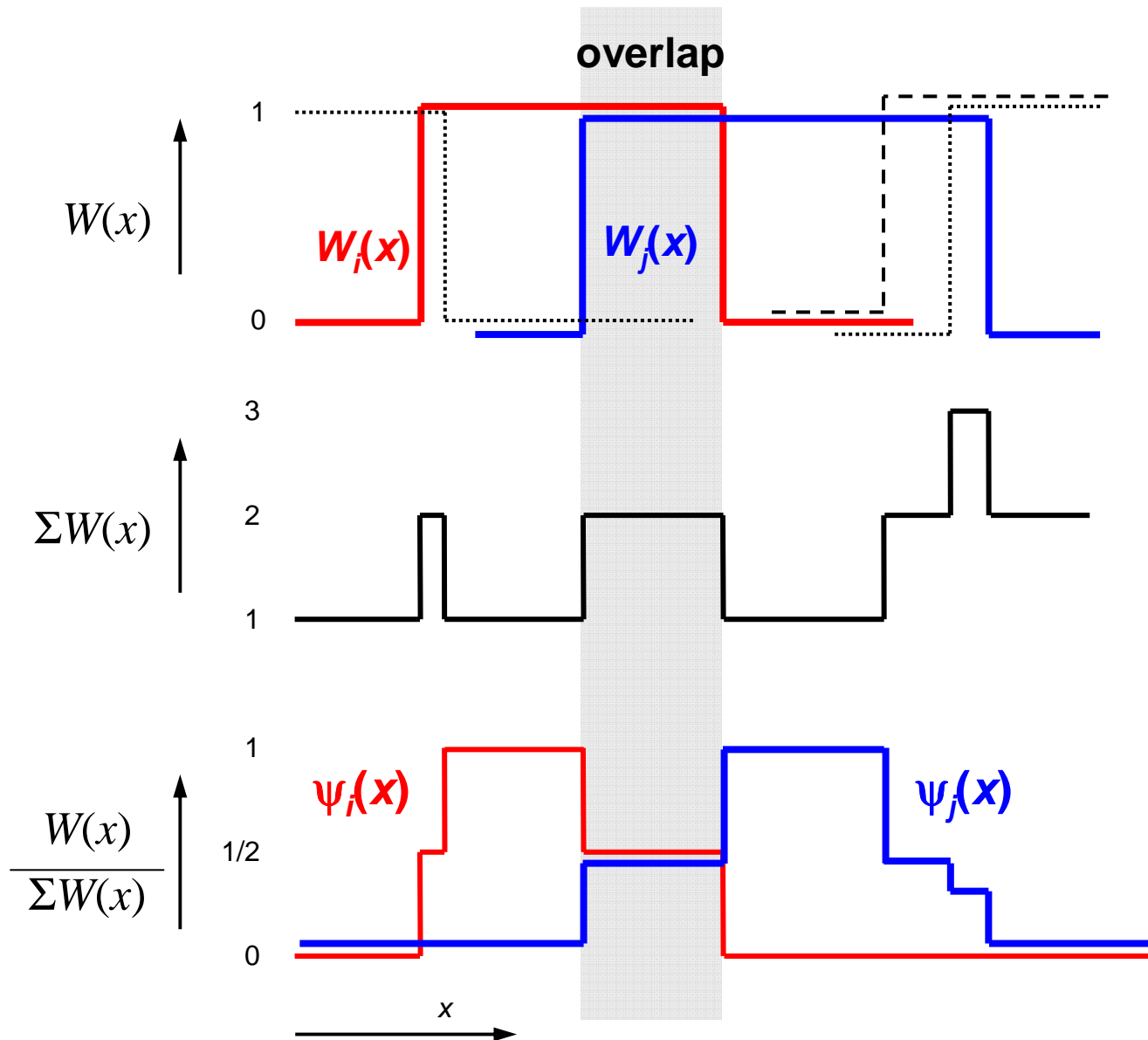
Smooth kernel functions



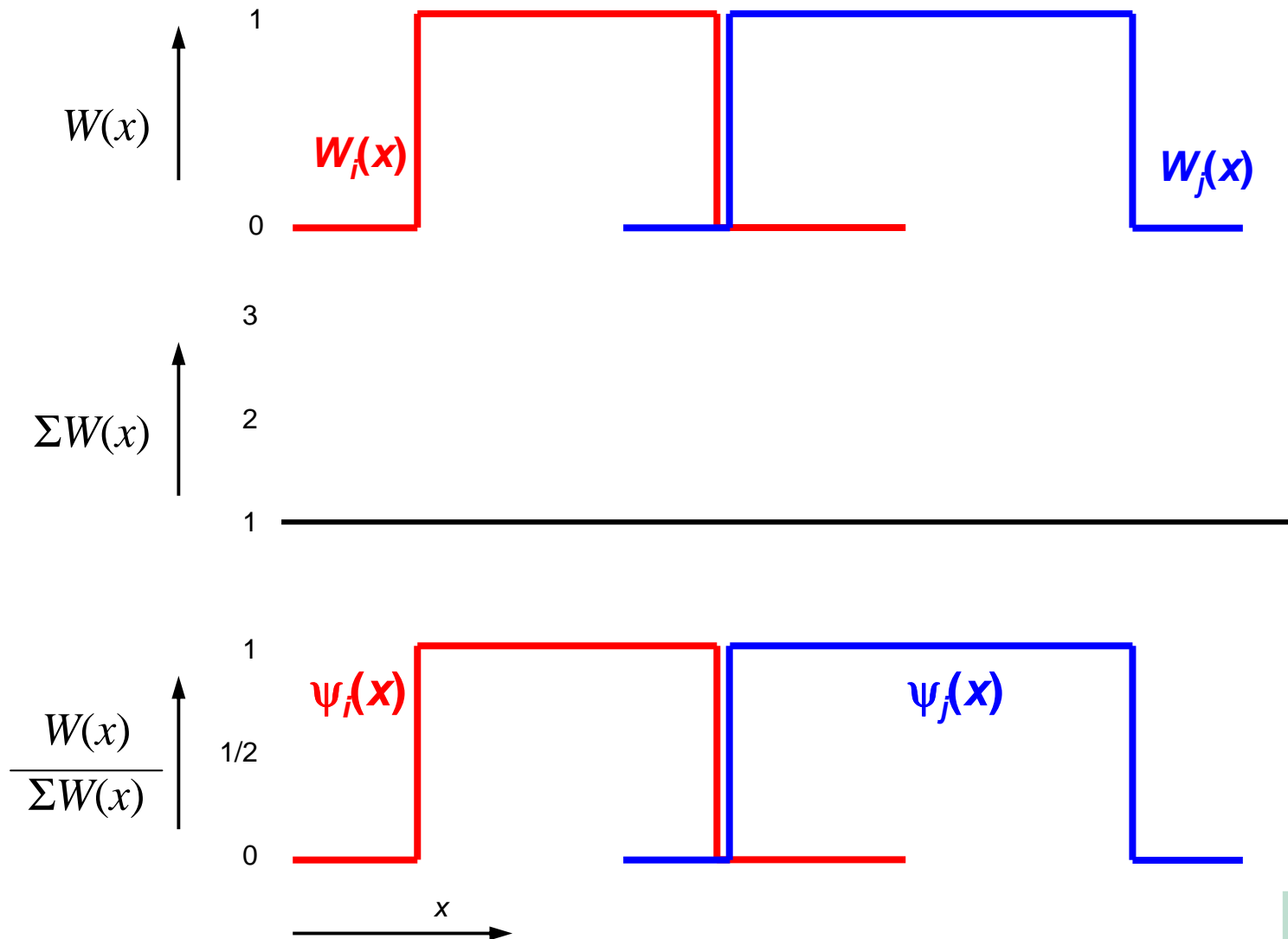
$$\beta_{ij} = \int \frac{W_i \nabla W_j - W_j \nabla W_i}{\left(\sum_k W_k(\mathbf{x}) \right)^2} d\mathbf{x}$$



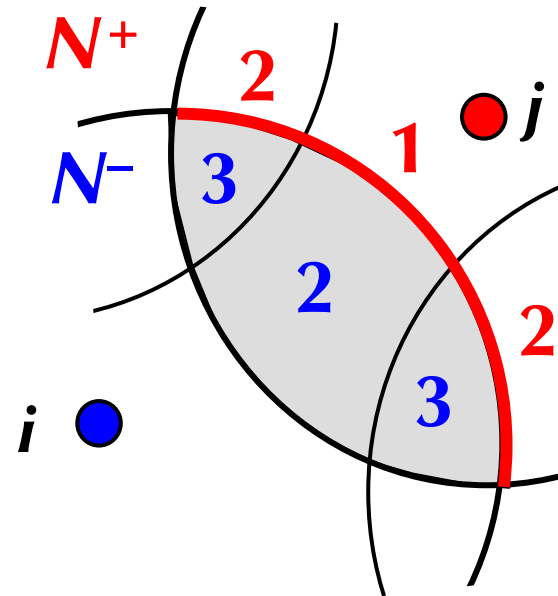
Top-hat kernel functions



Non-overlapping top-hats = mesh finite volume



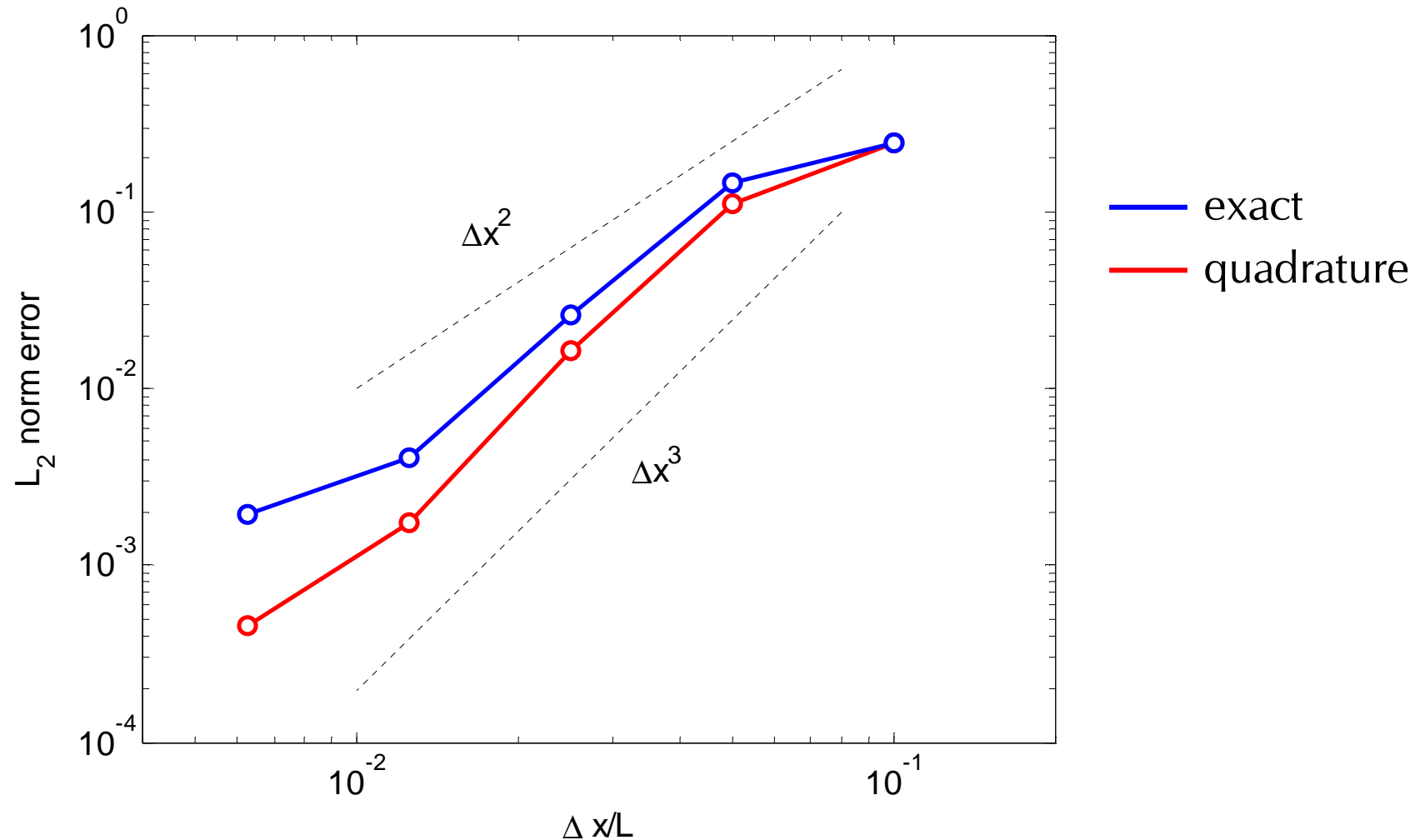
Evaluation of β_{ij} with overlap top-hat kernel



$$\int \frac{W_j \nabla W_i}{\left(\sum_k W_k(\mathbf{x}) \right)^2} d\mathbf{x} = \int \frac{W_j \nabla W_i}{N(\mathbf{x})^2} d\mathbf{x} = \int \left(\frac{1}{N^-(x)} - \frac{1}{N^+(x)} \right) \mathbf{n} ds$$

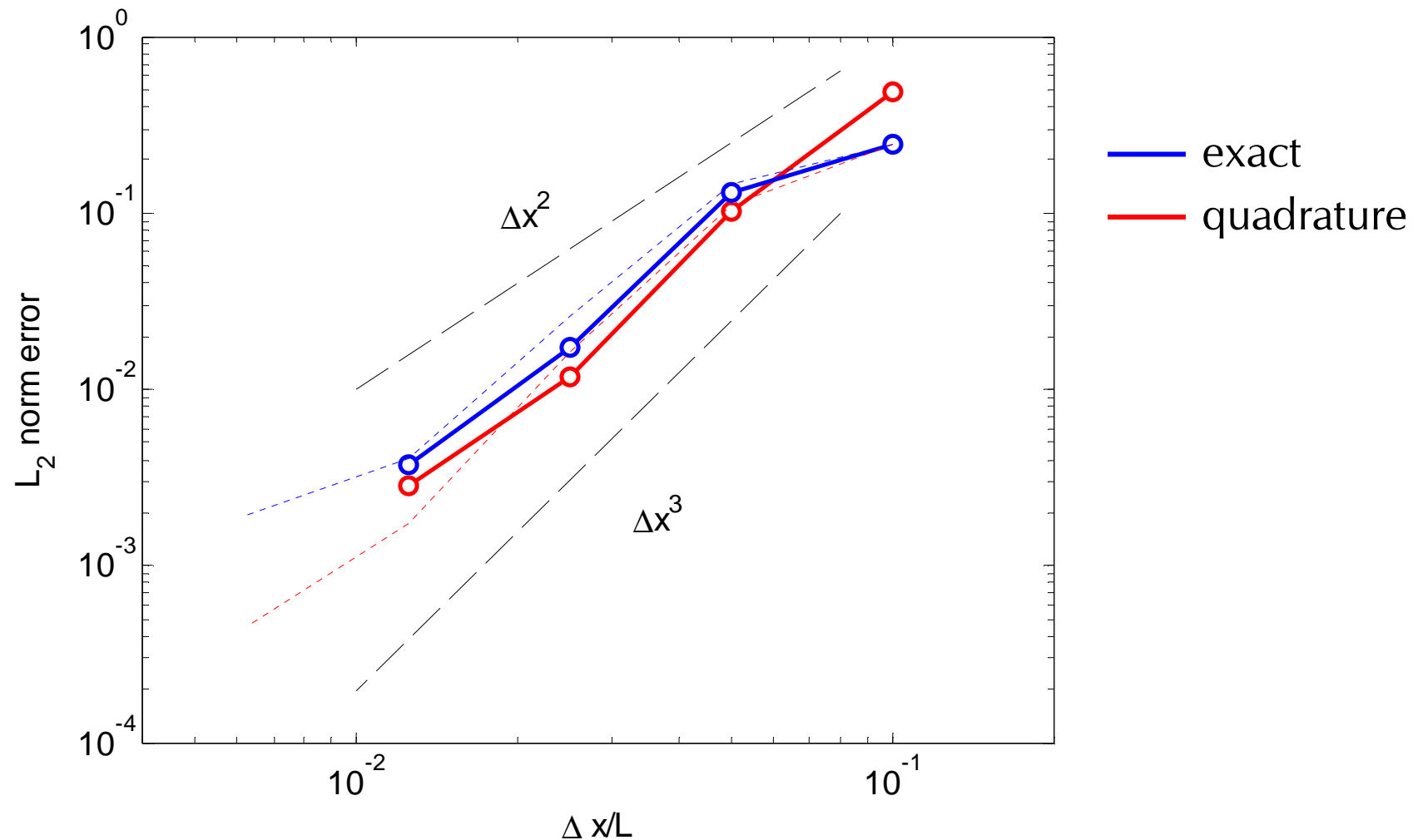


Comparison of integration methods



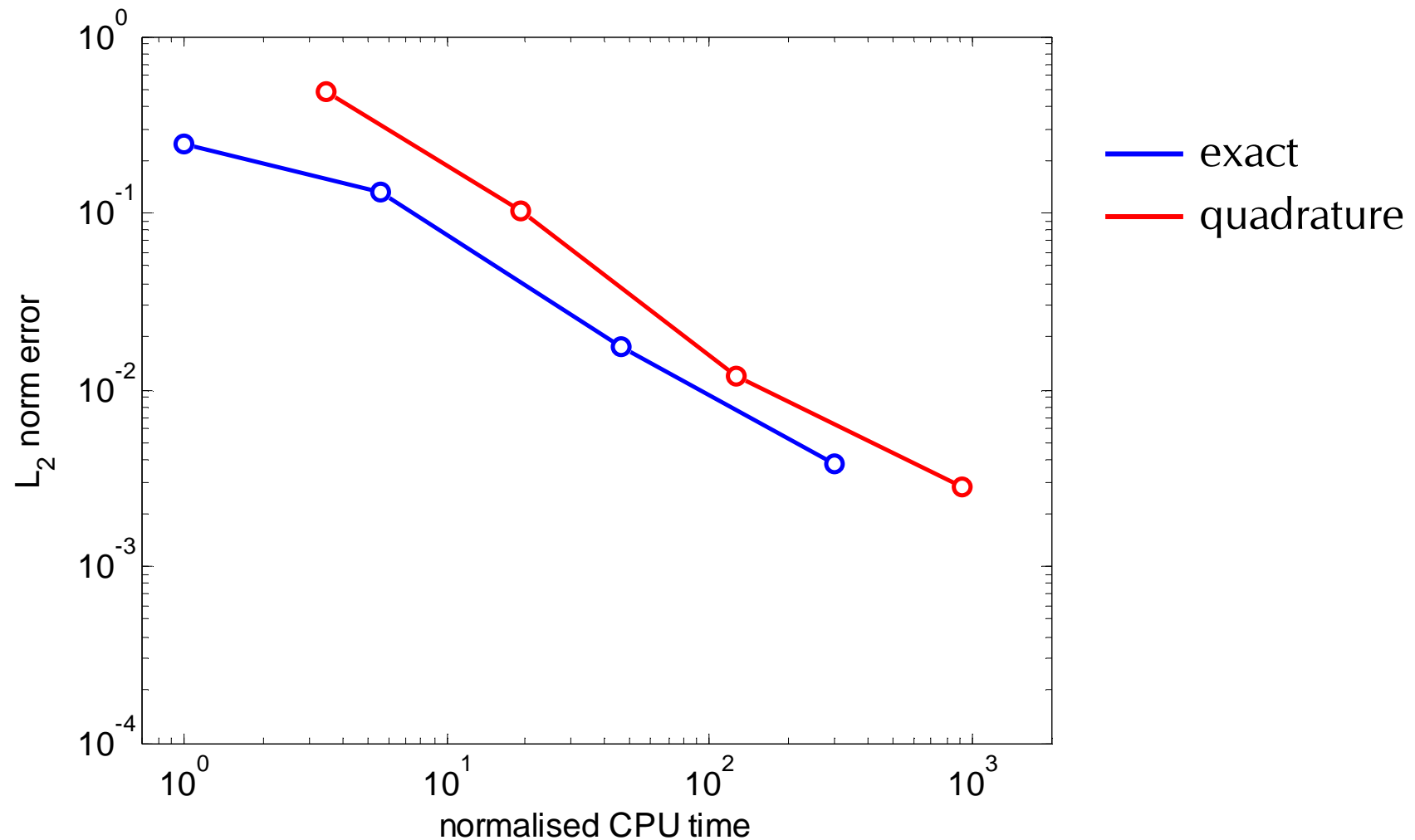
Taylor-Green flow
Re = 100, Eulerian particles

Comparison of integration methods



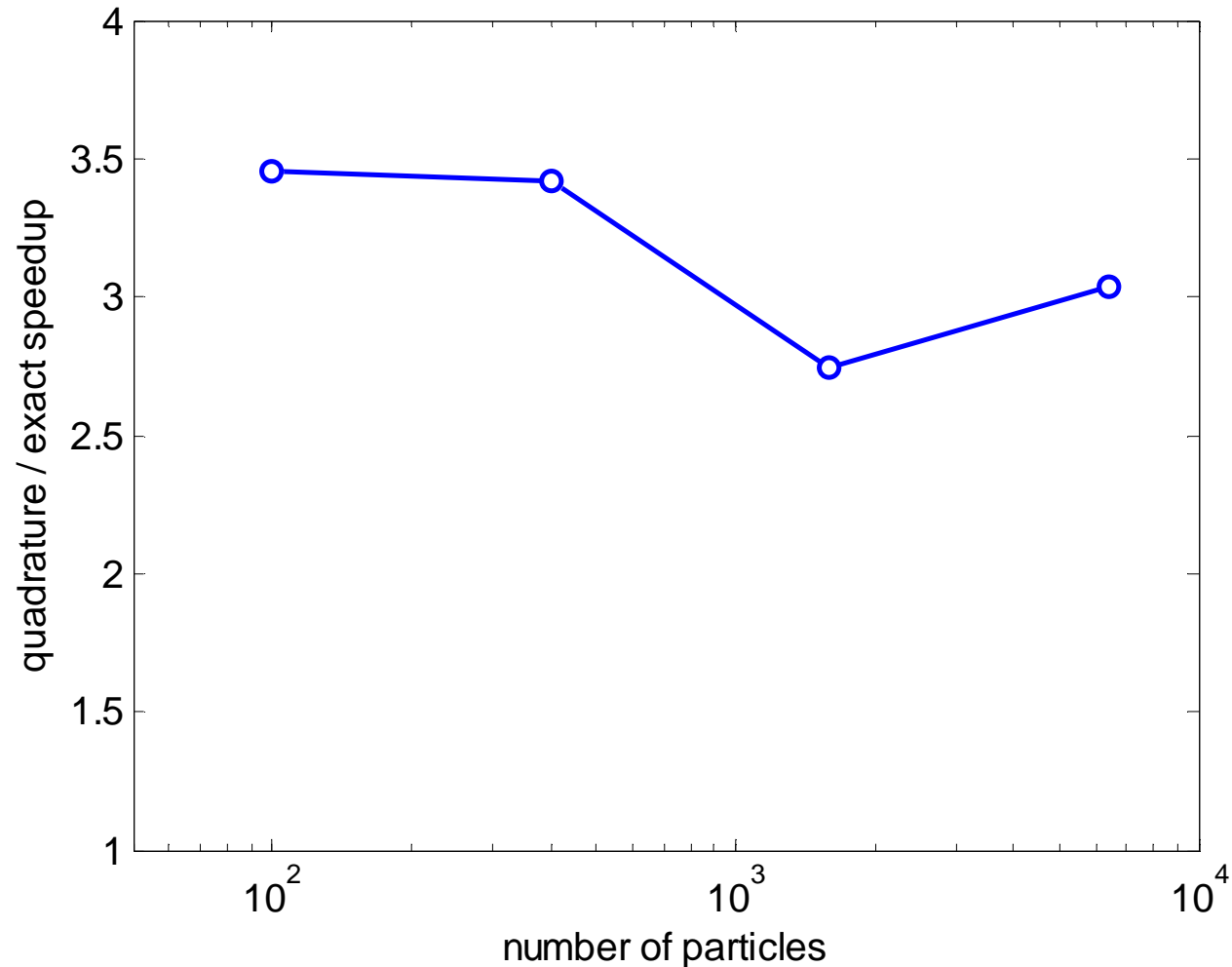
Taylor-Green flow
Re = 100, nearly Lagrangian particles

Comparison of integration methods



Taylor-Green flow
Re = 100, nearly Lagrangian particles

Comparison of integration methods



Taylor-Green flow
Re = 100, nearly Lagrangian particles

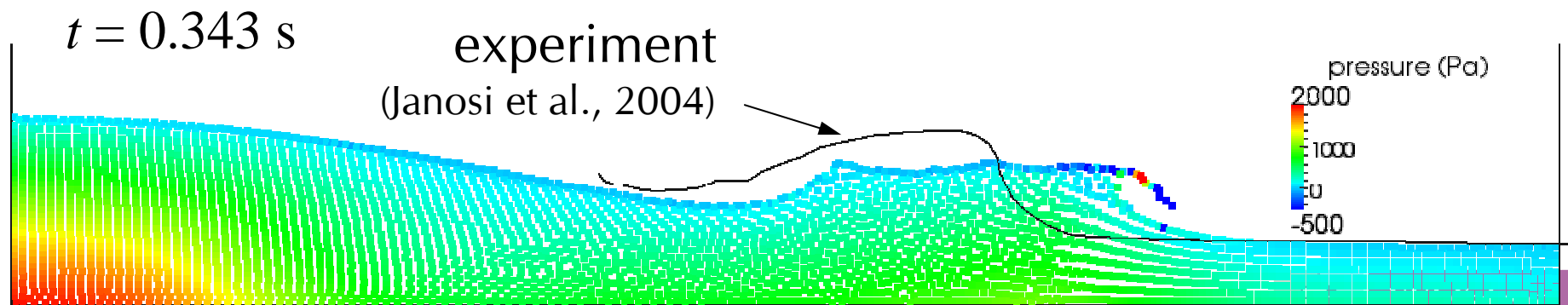
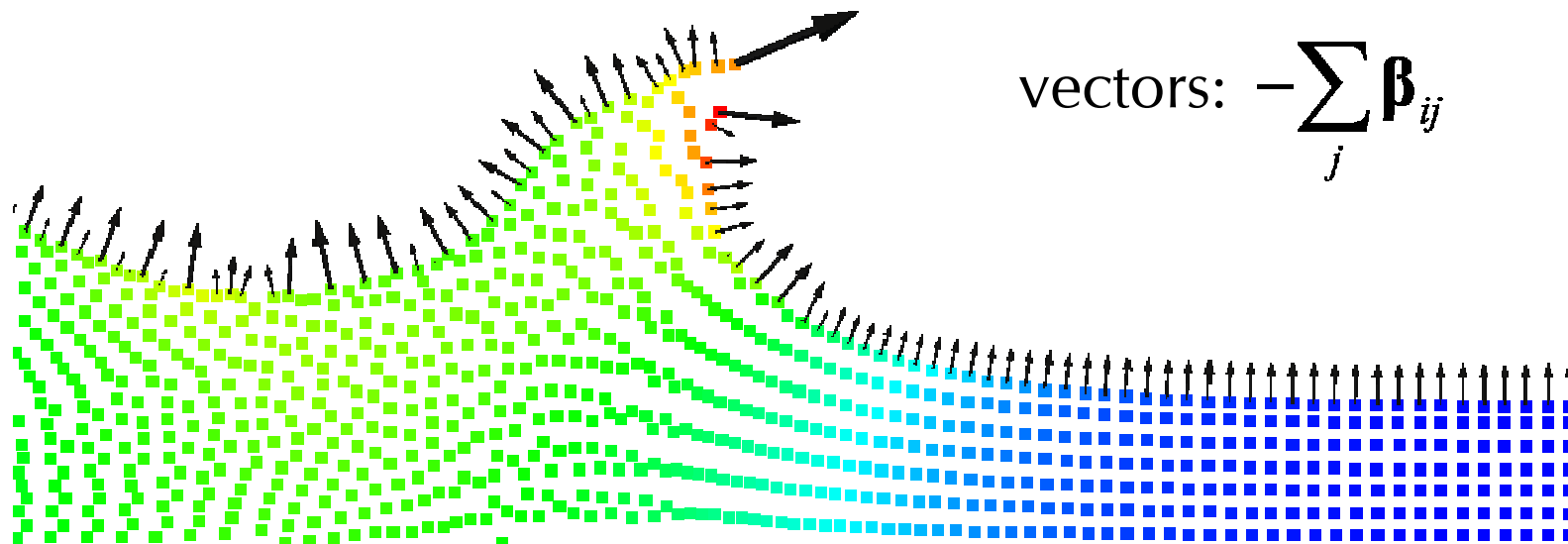


Kernels for FVPM: summary

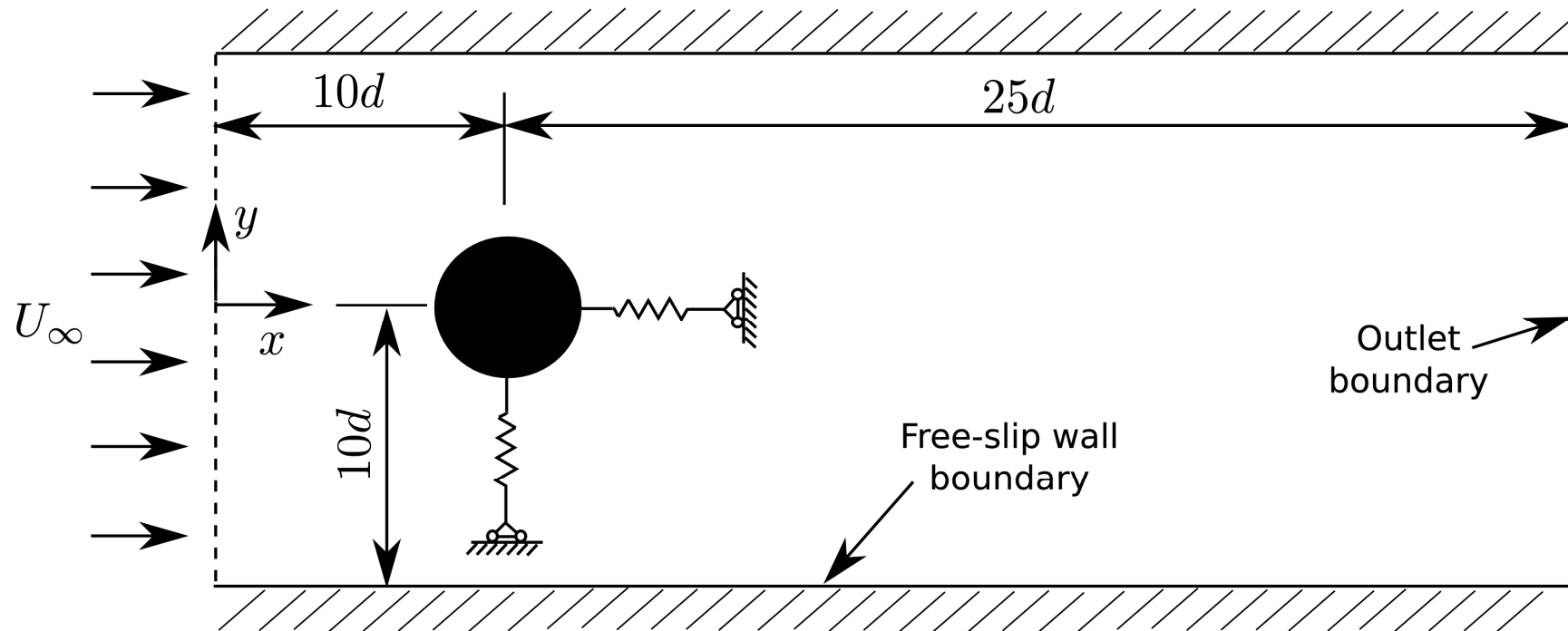


Exact β_{ij} enables free-surface modelling

SPHERIC benchmark 5



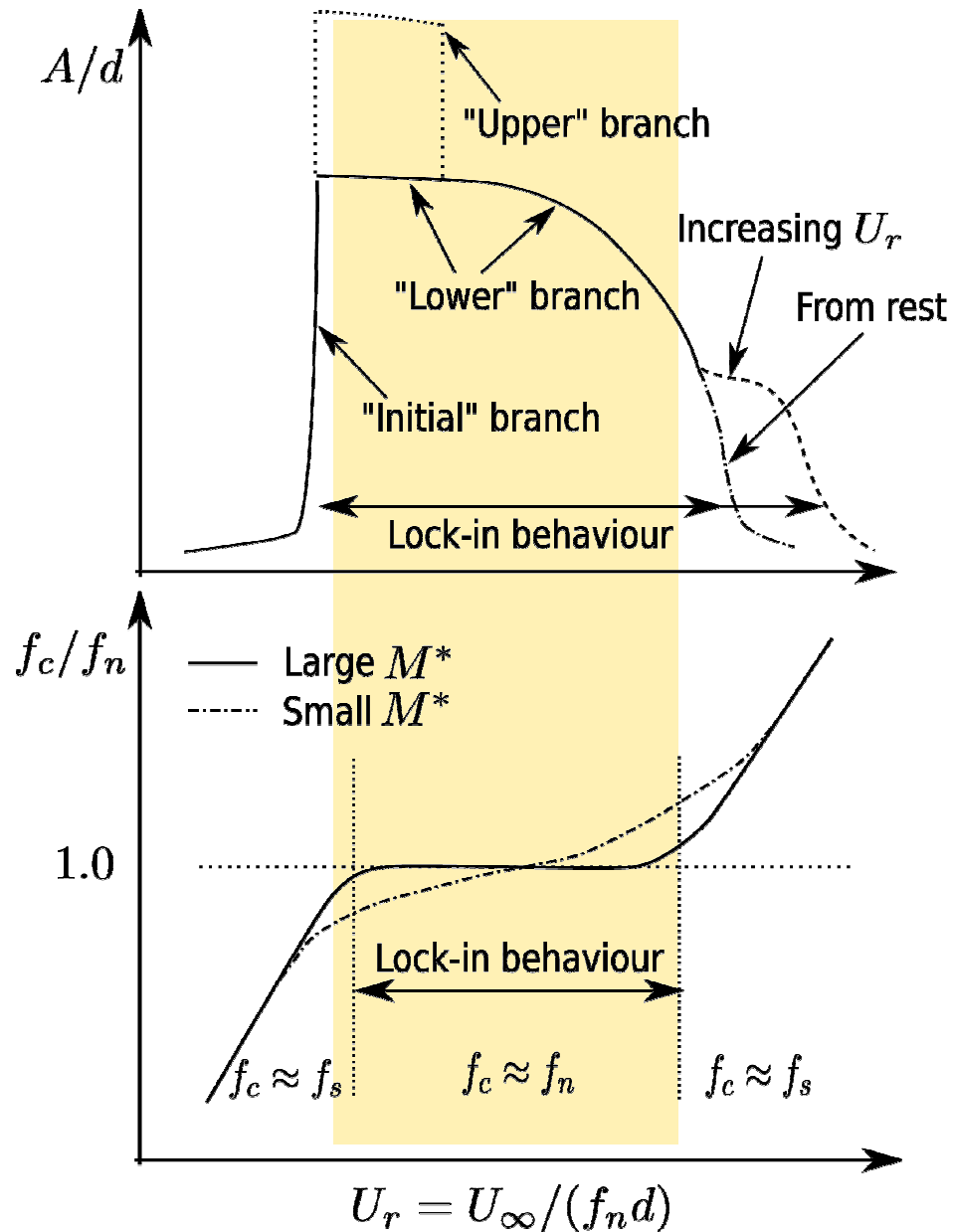
Vortex-induced vibration



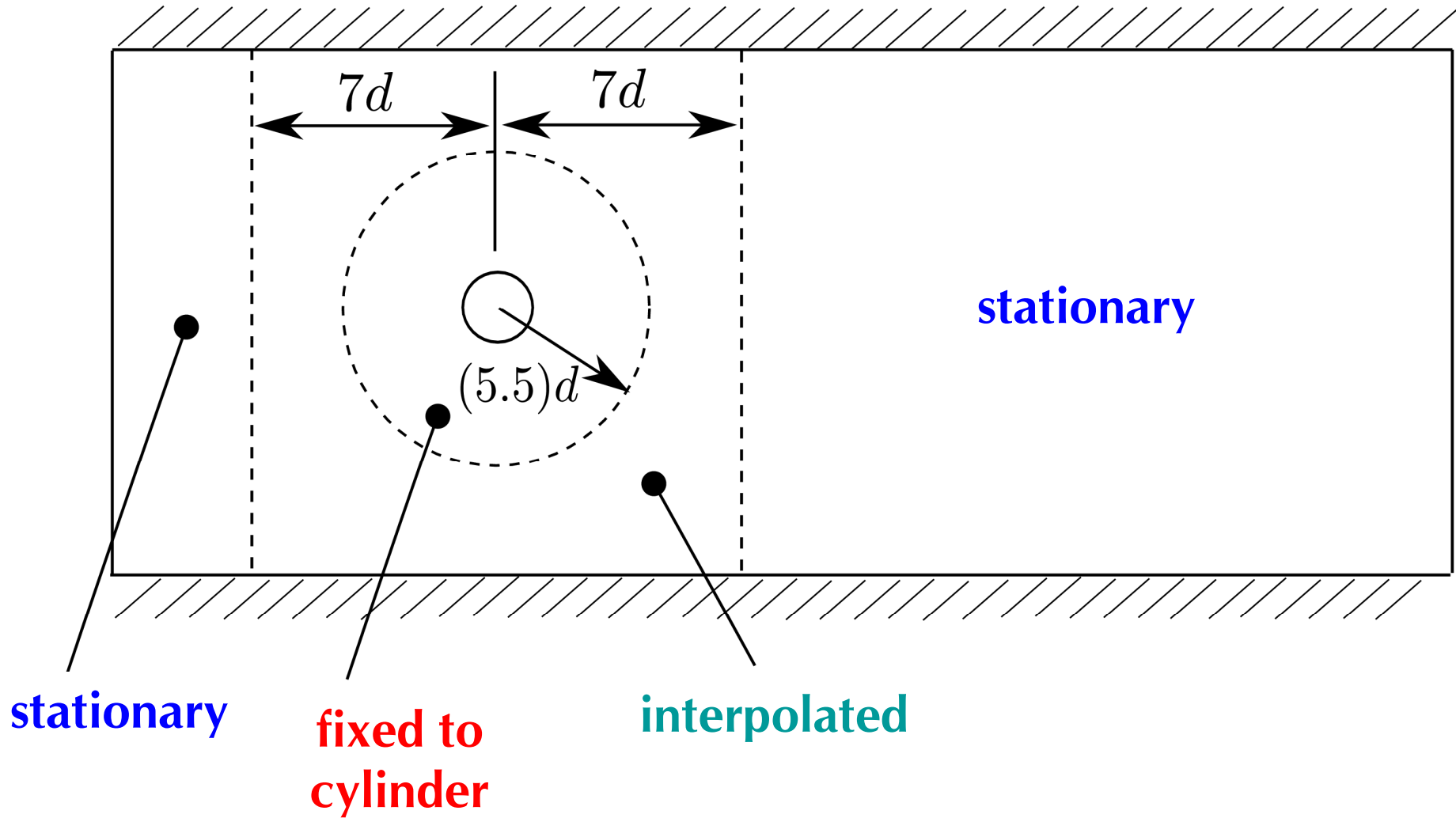
$$Re_d = 100$$



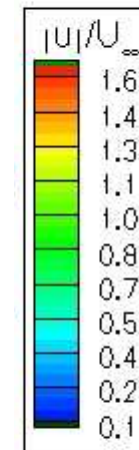
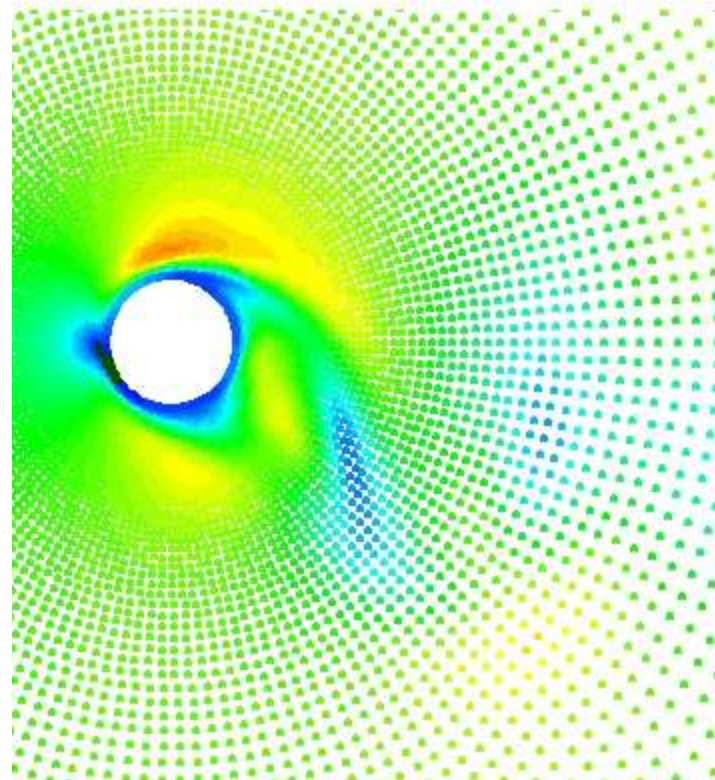
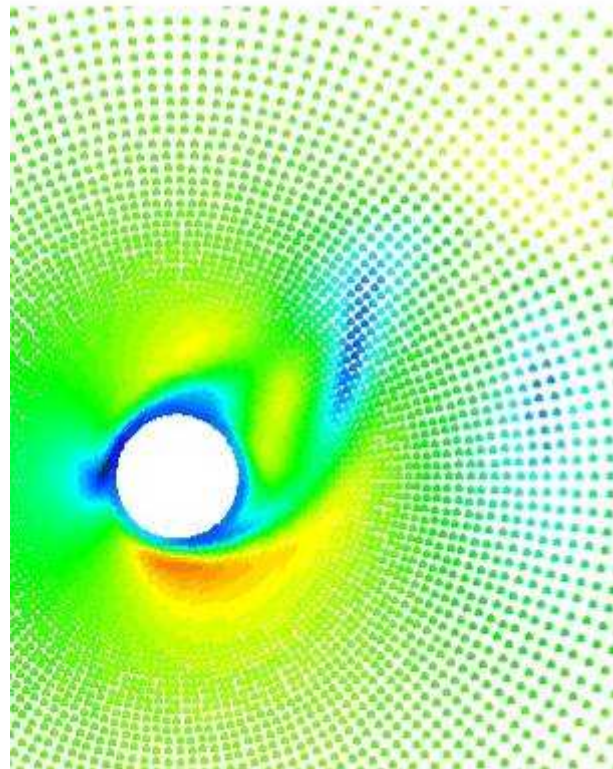
Vortex-induced vibration



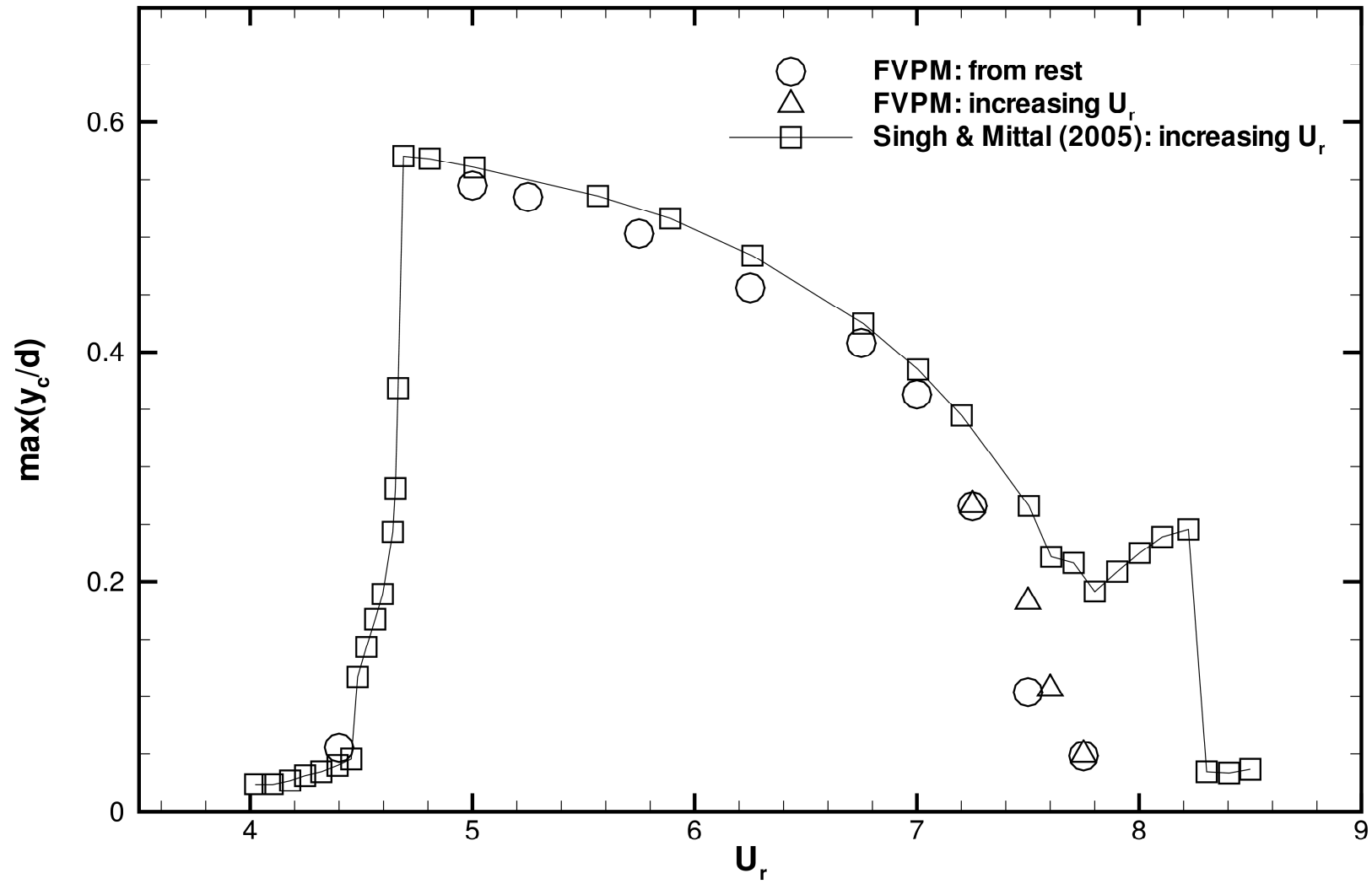
Particle motion schemes



Results



Results



Conclusions

- FVPM is closely linked to Riemann SPH
- FVPM gives robust, simple boundary treatments
- Exact interaction vectors yield $3 \times$ speedup
- Validated for bodies with prescribed and free motion

Future work

- Control of particle motion and distribution is critical
- Extension to 3D

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